

Program BA4

FOR CALCULATION OF ROOM TEMPERATURES
AND HEATING AND COOLING LOADS

USERS GUIDE

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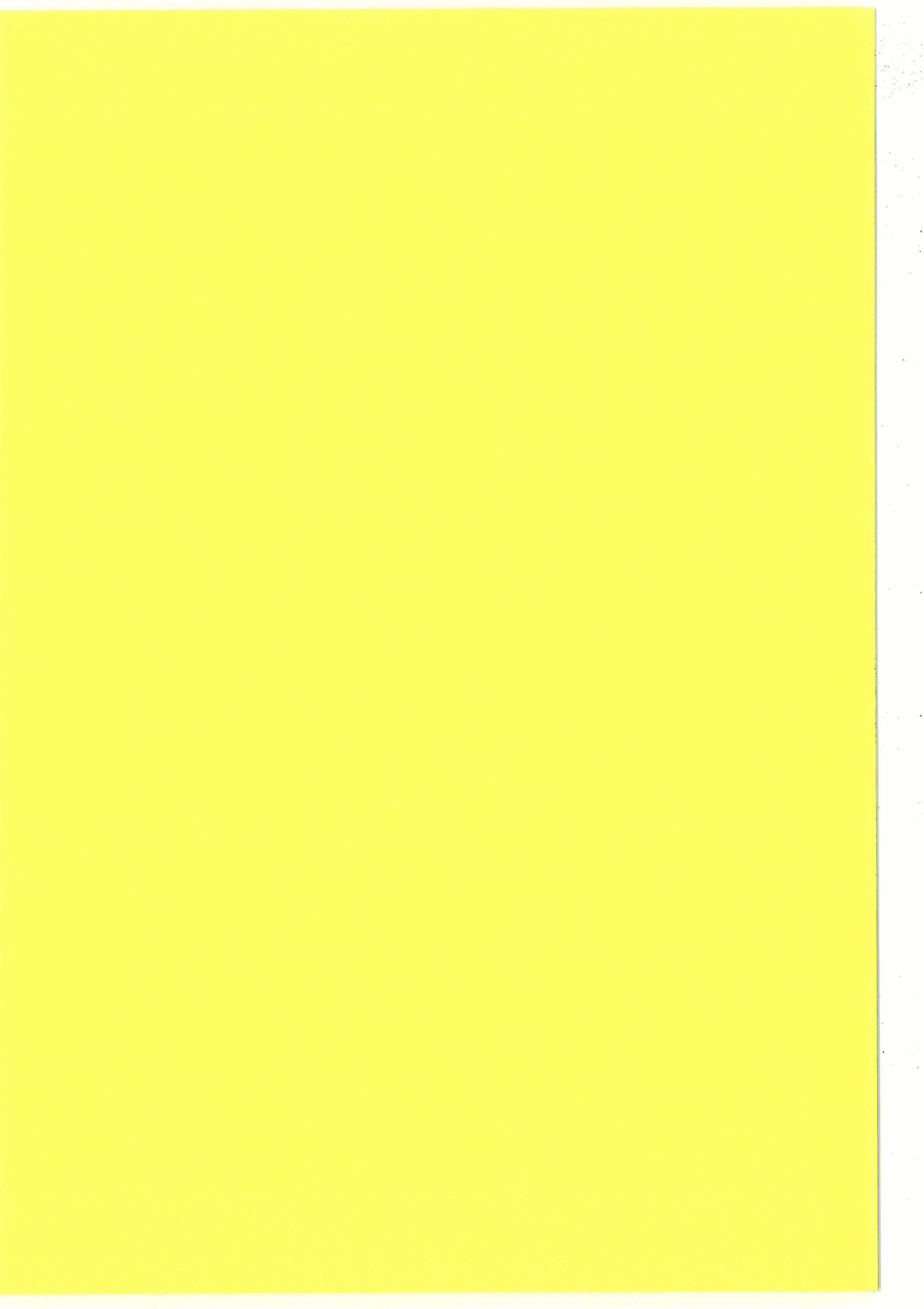


Report no. 44

THERMAL INSULATION LABORATORY

Technical University of Denmark

2. ed. 1979



PROGRAM BA4

for calculation of room temperatures
and heating and cooling loads.

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Preface to 2. edition.

Two extensions have been included in the BA4 programme, April 1977 version:

- 1) An option of running quasistationary conditions, with repeating diurnal cycle. Then the Test Reference Year is not used, and consequently sunradiation and outside air temperature have to be specified (BA2 type card, AIRTEMP 2 time serie, page 13).
- 2) The direct beam radiation in the Danish Reference Year can be zeroed on certain days in December, January, March and April, thereby bringing the direct radiation in better accordance with the average number of sunshine-hours in the months mentioned. (MODREF type card, page 13). This option shall be used only with the Danish Reference Year published 1974.

A short description of the programme can be found in:
Hans Lund: The model and theory behind the BA4 programme,
Thermal Insulation Laboratory, 1978.

January 1979

Hans Lund

Programme BA 4

The programme calculates for a room half-hour values during a whole year of room temperatures, utilizing a simplified method. Further it can calculate heating and cooling loads, taking into account sun radiation, fixed and movable sun shading devices, varying ventilation and infiltration, electric lighting and other heat sources in the room, etc.

The calculations utilize the weather data from the Danish Reference Year.

The results may be presented in several different ways, with a few values for each day, with detailed description for singular days, or for each of the twelve months and for the whole year, sums, mean values, frequencies or fractiles.

The main simplifications in the calculation method consists in:

- 1) that all surfaces in the room, apart from the window, are assumed to have the same surface temperature.
- 2) that all heat accumulation takes place in one layer inside the wall, and that the heat accumulating layers of all walls have the same temperature.
- 3) that all surface resistances are constant (but not necessarily equal).

The programme consists of one main programme and ten subroutines. Totally 1200 cards, including comments.

By using a condensed Reference Year stored on disc, the execution time will be 16-24 sec. for one room, one year, dependent of numbers of window orientations, sun shading devices etc.

(On an IBM 370/165 system, compiled by a FORTG compiler, compiling time not included, core needed: approx. 83 k + input-output buffers, total 98 k).

Programme BA 4 is developed at the Thermal Insulation Laboratory, the Technical University of Denmark. Special editions exist for certain purposes, and the programme is sometimes changed. This copy relates to May 76* status of the programme.

The method utilized is proposed and described by Bo Andersen.

The programme is owned by the Thermal Insulation Laboratory, the Technical University of Denmark, Building 118, 2800 Lyngby. It is supplied free to potential users.

May 1976

Hans Lund

*) This copy relates to the April 1977 version of the programme.

Test Reference Year

(Danish "Reference Year")

The "Test Reference Year" (TRY) is a weather data collection with 8760 hourly weather registrations, containing a considerable number of weather parameters for each hour. It is intended, for a given location, to ideally represent the weather throughout a typical year, on the assumption that a typical year can be defined.

Its main purposes are to make it possible for architects, consulting engineers, and others to make use of computing programs for calculations of energy consumption and indoor climate by an entire year of weather data, and to make it possible to compare different projects throughout a whole year.

For the program mentioned here, the Test Reference Year is normally used in a condensed form, stored on disc, and containing per hour those data only that are relevant to the program.

In those cases where a condensed Test Reference Year is not available, the full Test Reference Year on tape is utilized. The subroutine DISKL is then substituted by a subroutine TAPL (included in this version of the Users Guide). CALL TAPL instead of DISKL in line 106 in MAIN-programme.

For those cases where a Test Reference Year with hourly values of direct, normal radiation and diffuse radiation is not available, the Laboratory possesses algorithms and subroutines that permit calculations of the radiation data from cloud cover observations.

Output from BA 4 programme

The output covers:

- I A reproduction of input data.
- II A "small" list output with a few values for each day of the year.
- III A "big" list output with values for each half hour for a few (up to 10) specified days of the year.
- IV Monthly and yearly frequencies, mean values, sums or fractiles.

I and parts of IV are always produced.

II is produced if it is not specified suppressed.

III and the remaining part of IV have to be specified in order to be produced.

Each page in the output carries the job title from the title card and the date of the execution of job.

I Reproduction of input data. 2 pages.

After title of job follows on page 1 room data with data names. Besides the time interval $DT = 0.5$ (hour) is written. DT is a constant in the programme.

After that follows a list output of all recorded "type cards" and of the cards giving time series for ventilation and infiltration.

On page 2 are written out full time series (48 half-hour values) from:

AIRTEMP 1	desired room air temperature.
AIRTEMP 3	specified temperature of adjoining room, and
AIRTEMP 4	the temperature of the ventilating air, if this temperature is recorded with a time series. If it is derived from the outer air temperature it will here be zero (or, by repeated calculations, a value without meaning).
QMAX	maximum available heating effect
QMIN	maximum available cooling effect
FLUX	specified heat flows, however at least FLUX 10 (heat from electric lighting) and FLUX 1.

Further the daily sums of the individual FLUXes are written out, and the distribution KONvection and RADiation, i.e. to room air and to surfaces, of QMAX, QMIN and FLUXE.

When by means of a 999-card a new calculation follows after ending the first one, again all room data are written out on page 1, but only the type cards and time series which are specified for this new calculation. All other inputs are assumed unchanged from the first calculation.

Page 2 is written in full.

NB. This is not rather useful, as list output from the calculations cannot be separated from each other without losing information of complete input data. Therefore an alteration is being planned in order to write all input data for each calculation.

II "Small" list output.

Per 24 hours is printed out one line with:

MD	Month.
DG	Day.
RLT M	Daily mean of room air temperature.
KL	Hour for
RLTMAX	Daily maximum of room air temperature.
OP-T	Daily maximum (without indication of time) of operative temperature towards the inner walls of the room, if OPERative is specified.
OPTX	Daily maximum of operative temperature towards window wall with window nr. X, if OPERative X is specified.
UDT M	Daily mean of outer air temperature.
Q KOLE	Daily sum of cooling. If both QMIN with time series (for maintenance of AIRTEMP 1) and QMIN NB (for maintenance of the temperature NB °C) are specified, the daily sum is incorrect and invalid.
Q VARM	Daily sum of heat conveyed to the room to maintain AIRTEMP 1.
Q PRIM	Daily sum of heat conveyed to primary air.
Q SOL	Daily sum of heat from sun through window, outer wall and roof.
UVQ	Number of half-hours with either cooling to the temperature NB °C, or extra ventilation.
E-L	Number of half-hours with electric lighting.
B-AX	(X=1 through 4), number of half-hours with movable shading device for the windows nr. 1-4, if specified.

III "Big" list output.

For each day specified with "big" list output one page with 48 half-hour values from 0.30 to 24.00 is written.

RL-T	Room air temperature.
OP-T	Operative temperature towards the walls of the room.
OPTX	Operative temperature towards window wall with window no. X, if OPERativ X is specified. If X is not specified (or X=0), the caption will be OPT*, and the value given will be the operative temperature towards a double-pane without any sun radiation absorbed in the panes.
UDLT	Outer air temperature.
QREG	Heating or cooling effect conveyed to the room. If within a half-hour, cooling effect occurs to both QMIN with time series and to QMIN NB, only the last cooling effect, to the temperature NB, will be written out.
QPRIM	Heating or cooling effect conveyed to the ventilation air.
QTOT	Total heating effect.
SOLIND	Heat from sun radiation through windows.

- UVQ Indicator = 1, if within the half-hour there has been cooling to the specified temperature NB or extra ventilation, otherwise 0.
- E-L. Indicator = 1, if the electric light has been on.
- B-AX (X=1-4), indicator = 1, if movable shading device has been used at window X.

IV Monthly and yearly tables.

2-6 pages are written, dependent of the specification of OPERative.

a. Frequency of the room air temperature, as half-hours, divided into full degree intervals for the 12 months of the year and for the whole year. All 48 half-hours of the day are included and temperatures within the interval 12-40°C, and "below 12°C" and "above 40°C".

Further is written out monthly mean of the room air temperature, and the monthly sum of:

- QQ- Cooling to the room.
- QQ+ Heat to the room.
- QPRIM Heat for preheating of the ventilation air. (If AIRTEMP4 is specified with a time series, cooling of the primary air may occur at high outer air temperatures, reducing the sum QPRIM.
- QTOT Total heat effect QPRIM + QQ+.
- QSOL Total sun radiation through windows, walls and roof.
- QELYS Total heat from electric light.
- UVQ Number of half-hours either with cooling to the temperature NB or with extra ventilation.

Also the corresponding yearly values are written out, and at last the total heating load for the months October - April incl.

b. Frequency of the room air temperature during the working hours, i.e. during the 18 half-hours between 8.30 and 17.00, if no other time interval is specified.

Besides a fractile calculation which in the area 12-40°C gives the 10%, 50% and 90% fractile, i.e. the temperature under which this percentage of the half-hours is situated.

c. Frequency of the operative temperature for all half-hours of the day. This list output c and d is only calculated if OPERativ is specified.

d. Frequency of the operative temperature during the working hours.

In addition a fractile calculation.

e. Frequency of the operative temperature towards window wall during the working hours. This list output e and f is only calculated if OPERativ X is specified, where X is the number of a window specification (X = 1-10).

In addition a fractile calculation.

f. The difference between the operative temperature towards the window wall and towards the walls of the room during the working hours. Given as a frequency of half-hours in full degree intervals in the area -8°C to 20°C .

In addition a fractile calculation.

Input cards for BA4

The program operates in the SI-system of units. Output is given in kWh or W.

1. Title card. col. 1-72 job title. Is reproduced on output.
2. Room data. Arbitrary succession.
Col. 1-2: name, col. 3-12:value, with decimal point.
 TU Heat transfer from inside surface to outer air, for the window from room air to outer air.
W/°C.
 TK Heat transfer from inside surface to adjoining room with specified temperature (AIRTEMP 3), e.g. corridor.
 TO Heat transfer from room air to all inside surfaces.
 TA Heat transfer from inside surfaces to common accumulating layer.
 S The heat capacity of the common accumulation layer of the room. Wh/°C.
3. Blank card. Terminates room data.
4. Heat flows, air change, window data, output specifications etc. Arbitrary succession and number. Two types of cards can be used: "type cards" and "time series".

Type cards:

col 1-8 name (only col 1-4 are significant).
 col 10-11 number NB, integer, units in col 11.
 col 12-21 numerical value CK, with decimal point.
 col 22-31 numerical value CR, with decimal point.

Time series: consist of two or more cards:

col 1-5 hour and minute, with decimal point.
 col 11-20 numerical value, with decimal point.

The first card in a time series shall have the hour 0.00, the last card 24.00, and the numerical value for the two cards must be identical. Between them can be inserted cards for other hours. The half-hour values for the calculation appear by linear interpolation between the given hours.

Generally, if CK and CR both are equal to 0, the type card must be succeeded by a time series. If CK or CR or both are different from 0, no time series must follow.

Name	NB	
AIRTEMP	1	Desired room air temperature maintained by heating or cooling, given as time series.
AIRTEMP	3	Temperature in adjoining room or corridor, given as time series.
AIRTEMP	4	Temperature of the primary air to the room, given as time series,
		or
AIRTEMP	4	CK CR Temperature of the primary air follows the outer air temperature with TOVT=CK, temperature increase on primary air from fan and ducts, and TMIT=CR, minimum accepted primary air temperature (maintained through preheating if necessary).
FLUX	1 thru 9	Heat flow to the room, given as a time series. (W). Up to nine different heat flows.
FLUX	10	Heat flow to the room from electric illumination, operated on-off by the level of daylight from the window. Given as a time series.
FLUX	1 thru 10	CK CR CK and/or CR different from 0. CK is a factor for that part of the heat flow which is given off convectively direct to the room air. CR is a factor for that part which is radiated to the surfaces of the room. If CK and CR are not indicated for a FLUX it is assumed that the whole heat flow is radiation to the surfaces (CK=0., CR=1.).
QMAX		Maximum possible heating effect to the room, as a time series, for obtaining AIRTEMP 1.
QMAX		CK CR CK and/or CR not equal to 0. Factors for convective and radiative part of the heating effect. If nothing is specified, default values are CK=1., CR=0., i.e. purely convective.
QMIN		Maximum possible cooling effect to the room, as a time series, for obtaining AIRTEMP 1. (Given with minus sign).
QMIN		CK CR CK and/or CR different from 0. A factor for giving off convection and radiation, analogous to QMAX.
QMIN	NB	Cooling to the temperature NB. CK=CR=0 or blank. This typecard must be followed by a time series, the content of which is without importance, i.e. only the hours 0.00 and 24.00 need to be indicated. This cooling is calculated after any heating effect, there are no limits of the cooling effect, and it is exclusively conveyed to the room air. It makes it possible to specify a higher set-point for room air temperature (NB) by cooling than by heating (AIRTEMP 1).

OBS! MAXVENT and QMIN NB cannot be specified in the same calculation.

VENT NB Heat exchange by forced ventilation. Is given as a time series. The numerical value is in $W/^{\circ}C$, corresponding to the air change kg/sec multiplied by the (mean) specific heat of the air $J/kg^{\circ}C$. The ventilation is assumed to take place with AIRTEMP 4, which is given either as a time series, or following the outer air temperature without or with a preheating. VENT 0 (or blank) is valid all the year. VENT 1-10 is only valid for a period specified by:

VENT NB CK CR,
where NB $\neq$ 0, and CK and CR each have the form of a date (month.day) and indicates the first and the last day in the period with VENT NB. OBS! Here the succession is significant, as every new VENT for a given date substitutes the preceding, e.g. VENT 0.

INFILT NB Heat exchange by natural air change. Is given as a time series, analogous to VENT NB, only the air change takes place with outer air. (At the moment it is not taken into account that the natural air change is dependent of wind velocity or temperature differences). INFILT 0 (or blank) is valid all the year. INFILT 1-10 is only valid for a period specified with:

INFILT NB CK CR, analogous to VENT.

The following input data are only given as type cards (name, NB, CK, CR), without time series.

VINDUE NB CK CR
(window) NB = 1 through 10, up to 10 window specifications can be given. A "window" may consist of several, single windows with the same orientation. CK glass area, m^2 , total. CR window orientation, -180° to 180° (South= 0° , East= -90°). By the calculation of the sun radiation the window is regarded as double-glazed, 2-4 mm sheet glass, clear.

HORISONT NB CK
NB = 1 through 10. Indicates for window NB the altitude of horizon CK° . The horizon excludes by solar altitudes $< CK$ the direct sun radiation, but not the diffuse sky or ground reflected radiation.

FORMAT NB CK CR
Dimensions of one single window. NB = 1 through 10, indicates window number. CK = height of glass for one window. CR = width of glass - - -
FORMAT is to be specified if UDHAENG (projection) or RIBBE (rib) are specified. "Window NB" may consist of several identical individual windows.

UDHAENG NB CK CR
Shading projection over window NB. Reduces direct radiation and diffuse radiation. The canopy extends very long to both sides of the window.
CK height (in meters) of shading edge over the upper-edge of the window.
CR projection of shading edge in front of glass. (FORMAT for the window must be indicated).

RIBBE NB CK CR
Shading column, rib or wall edge next to window NB on both sides. Reduces direct radiation only.
CK distance (in meters) of shading edge from the nearest glass edge.
CR projection of shading edge in front of glass. (FORMAT for the window must be indicated).

BEV.AFSK NB CK CR
Inserts a sun shading device for the window NB, when the mean radiation on the window per m^2 is exceeding a limit value CK. The heat flow is thereby reduced by multiplication with the factor CR (the shading factor).

FORDEL NB CK CR
Distributes the sun radiation from window NB to room air and surfaces.
CK is the fraction of the sun radiation going to room air, when movable sun shading is not in use, the remaining part going to the surfaces.
CR is the fraction to room air when the movable sun shading is in use.
Default values are CK = 0.5, CR = 0.5.

VAEG NB CK CR
(wall)
Calculates the heat flow into the room arising from shortwave radiation on outer wall. The calculation is simplified, with a time delay and a transmission:
 $\alpha \cdot CK \cdot CR \cdot \mu$, where
 $\alpha = 0.85$ is the absorption coefficient for the exterior of the wall
CK = U-value of the wall
 μ = outside surface resistance, $0.05 \text{ m}^2 \text{ } ^\circ\text{C/W}$
CR = area of the wall in m^2 .
NB indicates a window number with the same orientation as the wall. Should there be no window with this orientation, a window with the area CK = 0. must be specified.
The time delay is obtained by assuming that 20% of the heat is getting through during the first half-hour, and that thereafter the heat flow decreases exponentially with 20% per half-hour. All heat is assumed supported to the inside surface.

TAG CK CR
(roof)
Calculates the heat flow into the room arising from sun on the roof. Analogous to VAEG.
CK ~ the U-value of the roof.
CR ~ the area of the roof.

B.ISOL CK
 Reduces the heat exchange TU with outer air through windows and outer walls, e.g. corresponding to insulation draperies or panels covering the windows.
 CK reduction factor for TU.
 The reduction takes place in the night at 18-7 during the period 28th Oct. to 9th April (day no. 301 to day no. 99), but any other conditions may be inserted (in MAIN).

ELLYS CK
 (elec.light) Conveys FLUX 10 to the room if the total sunlight through all windows is less than CK.

MAX-VENT CK CR
 Increases the air change in the room (e.g. corresponding to opening of window) if the room air temperature exceeds a given limit value. The increase of the air change takes place with outer air. The increase takes place only if the outer air is colder than the room air, and only to the extent which makes it necessary in order to decrease the room air temperature to the limit value.
 CK limit value for the room air temperature.
 CR total air change indicated as heat exchange in W/OC (analogous to VENT and INFILT).

OBS! MAX-VENT and QMIN NB may not be specified at the same time.

BA2 NB CK CR
 Causes the calculations made for quasi-stationary conditions. The Test Reference Year is not used, and outside air temperature must be specified with AIRTEMP 2, see below. Sunradiation is computed for day CK (month.day), with cloud cover NB (in okta's) and for latitude CR. For CR = 0 or blank, 56 deg. North is assumed.
 The calculations run 10 days, first and last day being printed out with half-hourly values ("Big" list output) and the others with one line only.

AIRTEMP 2 Outside air temperature, as time serie, like AIRTEMP 1, 3 and 4. To be used only after the BA2 type card.

The following input-data indicate the wanted presentation of output. If nothing is specified, the following is given:

- I A reproduction of input-data.
 Calculated time series at 0.30 to 24.00 of AIRTEMP 1, 3 and, if specified, 4, QMAX, QMIN, and FLUXes.
- II "Small" list output, that is 1 line per day with diverse temperatures, daily sums of heat flows and enumerations.
- IV The distribution of the room air temperature, monthly

and for the whole year, at 0-24, 8.30 - 17.00 (working hours) and monthly and yearly sums of different heat flows.

This can be altered by:

UDSKRIV CK CR
 CK = -1. or CR = -1. suppresses "small" list output. (Output II).
 CK og CR = month.day gives "big" list output for the date, i.e. for every half-hour: temperatures, heat flows and conditions for sun shading device, electric lighting etc.
 Up to 10 dates can be specified with big output (CK or CR = -1 takes the space for one date).
 Arbitrary succession. (Output III).

A-TID CK CR
 Alters the "built-in" working hours (as indicated under output IV) to the time from CK to CR.

OPERativ NB CK
 Leads to calculation of operative temperature (as the mean value of air temperature and surface temperature of walls). Is written out monthly and for the whole year, like IV.
 For NB $\neq$ 0 is also calculated the operative temperature towards the window wall with VINDUE NB, by which is included that the wall occupies the fraction CK of the total half room seen from the place in the room from where the operative temperature is wanted.
 The operative temperature is calculated for the working hours, and so is the difference between operative temperature towards the window wall and towards the inside walls of the room.

A special card to be used in connection with the Danish Reference Year only is:
 MODREF Causes direct (beam) radiation to be zeroed on certain days, because the number of hours with clear sun is too large in the Danish Reference Year in those months. The days are January 12, 14, 16, 17, 18, March 18, 19, April 17, 18 and December 1, 13, 14, 15, 20. No time series follows.

5. LASTFLUX-card (col 1-8) indicates that the input cards have ended, and the calculation may begin. After LASTFLUX shall be placed a blank card.
6. Succeeding calculations. Are obtained by inserting a card 999 in col 1-3 after LASTFLUX instead of a blank card.
 After that new room data follow. Cards are only inserted for the data which are to be changed as indicated under 2.
 After that a blank card is inserted as indicated under 3.
 After that new type cards and any time series follow as indicated under 4.
 Ending with LASTFLUX and blank card, or 999-card if one more calculation has to be run.
 Generally, by more calculations after each other, those data which are not expressly altered are carried unchanged to the next calculation.

MAIN, the main programme

The main programme contains the programme administration, including call of most subroutines, and the central procedure of calculation.

The succession is:

Initializing, i.e. recording of title cards, call of date, and zeroing of all variables, which are not zeroed for each day. This especially goes for the input data recorded through RUMDAT. Some data are given a value different from 0, which are then kept if another value is not recorded in RUMDAT.

Recording through RUMDAT (and EIND and SFLUX) of input data.

Initializing of data before start of a new calculation.

Calculation of the coefficients A1 and A2 for the temperature in the heat accumulating layer.

Recording of one day's weather data from Reference Year in subroutine DISKL (or TAPL), calculation for the day of the angles of the sun in SUNR, calculation of sun radiation through windows, walls and roof in SOLIN, and interpolation to 48 half-hours' values for outer air temperature and ventilation air, if any, in INPOL.

Initializing of data for the day, code for ventilation and infiltration, transmission of calculated values at 24.00 the prededing day to 0.00 for the day which is now calculated.

Output of table headings for "big" output, if any.

Start of half-hours-loop.

Calculation of additional insulation, if any, during winter nights.

Calculation of coefficients B and C for surface temperature and room air temperature.

Summing up of sunlight and of the total heat of the sun, per half-hour.

Switching in electric light, if any, at low levels of sunlight.

Calculation of temperatures without cooling or heating effect.

Calculation of necessary cooling or heating loads to maintain the desired room air temperature AIRTEMP 1.

Calculation of new temperatures with the available cooling or heating effect.

Calculation of extra cooling loads, if any, for maintenance of the room air temperature NB.

Calculation of new temperatures with the latest calculated, extra cooling effect.

Switching in extra ventilation if the room air temperature is above the wanted maximum, and if the outer air or ventilation air is cooler, and if extra ventilation is specified and is higher than the actually used ventilation for the half-hour.

Calculation of new temperatures with the extra air change, and the time ($\sim$ fraction of the half-hour) in which shall be extra ventilated to keep the temperature below the specified maximum. (Printout of this time is at present omitted).

Calculation of the inside, apparent radiation temperature of the window. (This calculation of which part of it is placed in SOLIN, is uncertain, as it is not clear what reasonably shall be included. Here it is assumed that the measuring area for the radiation temperature of the window does not receive direct sunradiation).

Calculation of operative temperature towards the walls of the room, and towards window wall, of which a part is opaque.

Enumeration of number of half-hours with extra cooling, extra air change, electric lighting, or with movable sun shading device for window 1 thru 4.

"Big" list output, if specified, one line with half-hour values printed.

End of half-hour-loop.

Print out of table heading for "small" output, after change of page in output.

Distribution and enumeration for monthly and yearly tables, including call of ADM 2.

Printout of line with "small" output, daily values, if this output is not suppressed.

If the date is not 31st December, return to DISKL to get weather data for the next day, etc.

If the day is 31st December, call subroutine UDSKR for output of monthly and yearly tables, fractile calculations, etc.

Reading of a new card. If it is a 999-card, return to call of RUMDAT and new calculation, otherwise calculations are stopped here.

Algorithms used in BA4, MAIN

The main program MAIN as a steering program contains calls for most of the subroutines. Besides, in MAIN is placed the central calculation procedure which every half-hour calculates temperatures, heating and cooling effects, or, if specified, increase of ventilation and electric lighting.

1. Formulae:

Heat accumulating layers, the temperature of the Nth half-hour, $N = 1$ to 48:

$$THA(N) = A1 \cdot THA(N-1) + A2 \cdot THO(N-1)$$

Surface temperature:

$$\begin{aligned} THO(N) = & B1 \cdot THA(N) + B2 \cdot TEXTI(3,N) \\ & + B3 \cdot TEXTI(2,N) + B4 \cdot TEXTI(4,N) \\ & + B5 \cdot QK(N) + B6 \cdot QR(N) \end{aligned}$$

Room air temperature:

$$THR(N) = C1 \cdot THO(N) + C2 \cdot TEXTI(4,N) + C3 \cdot QK(N)$$

where

TEXTI(2,N)	outer air temperature
TEXTI(3,N)	(specified) temperature of adjoining room
TEXTI(4,N)	temperature of ventilation air
QK(N)	heat conveyed to room air
QR(N)	heat conveyed to surfaces (radiation)

The single items can be split, e.g. if there are more than one quantity of ventilation air, with different temperatures.

2. Coefficients for calculation of temperatures: Accumulating layers:

$$A2 = \frac{TA \cdot DT}{ST} = \frac{TA \cdot 0.5}{ST}$$

$$A1 = 1 - A2$$

Here the half-hour cycle starts.

Intermediate values:

Total instantaneous air change.

$$\begin{aligned} VTSUM &= VENT(N) + INFL(N) \\ VTO &= 1 + VTSUM/TO \end{aligned}$$

3. Coefficients for calculation of temperature of surfaces:

$$\begin{aligned} B5 &= 1 / ((TA + TK + TU) \cdot VTO + VTSUM) \\ B4 &= B5 \cdot VENT(N) \end{aligned}$$

(The corresponding value for infiltration is integrated in the expression, $B5 \cdot INFL(N)$).

$$B6 = B5 \cdot VTO$$

($B1 = B6 \cdot TA$, $B2 = B6 \cdot TK$, $B3 = B6 \cdot TU$ are integrated in the expressions).

Auxiliary values:

$$RB5 = 1/B5$$

4. Coefficients for calculation of room air temperature:

$$C1 = 1/VTO$$

$$C3 = 1/(TO + VTSUM)$$

$$RC3 = 1/C3$$

($C2 = 1 - C1$ is integrated in the expression).

5. Calculation of new temperatures and heating or cooling.

Temperature of accumulating layers:

$$THA(J) = THA(J-1) \cdot A1 + THO(J-1) \cdot A2$$

where $J = 2$ to 49 .

Preliminarily calculated surface temperature:

$$\begin{aligned} THOJ = & THA(J) \cdot B1 + TEXI(2, J-1) \cdot B3 \\ & + TEXI(3, J-1) \cdot B2 + TEXI(4, J-1) \cdot B4 \\ & + TEXI(2, J-1) \cdot B5 \cdot INFL(J-1) \\ & + QK(J-1) \cdot B5 + QR(J-1) \cdot B6 \end{aligned}$$

First step of calculation of air temperature:

$$\begin{aligned} TBAS = & TEXI(2, J-1) \cdot C3 \cdot INFL(J-1) \\ & + TEXI(4, J-1) \cdot C3 \cdot VENT(J-1) \\ & + QK(J-1) \cdot C1/TO \end{aligned}$$

Preliminarily calculated air temperature, without regulation (heating or cooling):

$$TBAS + THOJ \cdot C1$$

Desired change of temperature by regulation:

$$TREG = TEXI(1, J-1) - TBAS - THOJ \cdot C1$$

To this corresponds a temporarily calculated regulating effect to the room air:

$$QREG = TREG \cdot TO/C1$$

Total regulating effect: $QQ(J) = QREG/CKK$.

New calculation in which is considered the influence of the regulating effect on the surface temperature, and thereby back on air temperature and TREG:

$Q_{REG} = Q_{REG} / (1 + (B6 \cdot CRR / CKK + B5) \cdot T_O)$,
where CRR and CKK are the fractions of the regulating effect delivered by radiation and by convection. ($CRR + CKK = 1$).

If Q_{REG} exceeds the part of the available heating and cooling effect delivered by convection, the convectively available effect is used in calculation instead.

Final surface temperature with regulating effect:

$$THO(J) = THOJ + QQ(J) \cdot (CRR \cdot B6 + CKK \cdot B5)$$

Final air temperature with regulating effect:

$$THR(J) = TBAS + THO(J) \cdot C1 + QQ(J) \cdot CKK \cdot CK / T_O$$

6. Limitation of temperature by cooling of room air.

Desired change of air temperature to TLIM:

$$T_{REG} = T_{LIM} - THR(J)$$

Necessary cooling effect (convective only):

$$Q_{LIM} = T_{REG} \cdot T_O / (C1 + B5 \cdot T_O) \quad (Q_{LIM} \text{ negative})$$

New surface temperature:

$$THO(J) = THO(J) + Q_{LIM} \cdot B5$$

New room air temperature:

$$THR(J) = THR(J) + Q_{LIM} \cdot (C3 + B5 \cdot C1)$$

7. Limitation of temperature by increased air change.

With outer air (NVU=2) or ventilation air (NVU=4).

Increased air change only if $TEXI(NVU, J-1) < THR(J)$.

VVV maximum air change, VVN increase from normal air change by ventilation

$$VVN = VVV - VENT(J-1) \quad TVV = VVN$$

New air temperature:

$$THR1 = THR(J) / C3 + TEXI(NVU, J-1) \cdot VVN / (VVN + 1/C3)$$

If $THR1$ is lower than the desired maximum temperature $TVMAX$, TVV is reduced proportionally:

$$TVV = (THR(J) - TVMAX) \cdot (T_O + VTSUM) / (TVMAX - TEXI(NVU, J-1))$$

and new THR(J) is set equal to TVMAX.

After that new VTSUM, VTO, B5, B6, THO(J) are calculated.

8. The heating load for heating the primary air excl. the over-temperature TOVT arising from fan and ducts, in each time interval:

$$Q_{\text{PRIM}} = (\text{TEXI}(4, J-1) - \text{TEXI}(2, J-1) - \text{TOVT}) \cdot \text{VENT}(J-1)$$

9. Calculation of the radiant temperature of the inside of the window. TVIN(J) is calculated in SOLIN as the temperature increase of the window caused by absorbed solar radiation:

$$\text{TVINJ} = \text{TVIN}(J) + (\text{THR}(J) + \text{THO}(J)) \cdot 0.625/2. + \text{TEXI}(2, J-1) \cdot 0.375$$

This expression is valid only for an ordinary double glass or thermopane.

Calculation of the indoor mean temperature of window and exterior wall. The wall occupies the fraction PRON of the half sphere visible from that position in the room where the directional operative temperature is wanted:

$$\text{TVIN}(J) = \text{TVINJ} \cdot (1. - \text{PRON}) + \text{THO}(J) \cdot \text{PRON}$$

Blank COMMON

MAIN, UDSKR, INPOL, RUMDAT, SFLUX

				To be read or calculated in	To be used in
TEKST (18)	Job title, 0-72 characters (=Z(18) in UDSKR, RUMDAT and SFLUX, =T(18) in INPOL)			MAIN	MAIN, UDSKR, SFLUX
QQ (50)	Regulating effect.	Half-hour values		-	MAIN
QK (50)	Total effect to room air	-	-	-	-
QR (50)	Total effect to surfaces	-	-	-	-
QMAX (50)	Maximum heating effect	-	-	RUMDAT	-
QMIN (50)	Maximum cooling effect	-	-	-	-
TEXI (4,50)	Four air temperatures	-	-	-	-
	1 Desired room air temp.			-	
	2 Outer air temp.			INPOL	
	3 Air temp. in adjoining room			RUMDAT	
	4 Ventilation air temp.			{ RUMDAT or INPOL	
INFL (12,50)	Natural air change	-	-	RUMDAT	-
	12 different ones				
VENT (12,50)	Air change by ventilation	-	-	-	-
COK (10)	Fraction of FLUX (1-10) supplied convectively			-	-
COR (10)	Fraction of FLUX (1-10) supplied by radiation			-	-
QLYS (10)	Heat from elec. light. Half-hour values			-	-

<u>COMMON/KORS/</u>		SOLIN, INPOL, SUNR, DISKL		To be read or calculated in	To be used in
AS (50)	Azimuth of the sun, half-hour values			SUNR	SOLIN
H (50)	Height of the sun, - - -			-	-
RNT (24)	Normal radiation from Ref.Year, hour values			DISKL	-
RDT (24)	Diffuse radiation - - - , - - -			-	-
TT (24)	Air temperature - - - , - - -			-	INPOL
FF (24)	Wind velocity - - - , - - -			-	not used
SO	Sunrise			SUNR	SOLIN
SN	Sunset			-	-
RTOT(24)	Total radiation from Ref.Year, is not used			DISKL	not used
TD (24)	Dew point temp. - - - , - - -			-	-
NN (24)	Cloud cover - - - , hour values			-	SOLIN
<u>COMMON/SR/</u>		SOLIN, RUMDAT			
HORM (10)	Demarcation of horizon, altitude, window no.1-10			RUMDAT	SOLIN
VAEK (10)	Outer wall,U-value•area, (with - - -)			-	-
UDHM (2,10)	Projection, height, overhang, at - - -			-	-
RIBM (2,10)	Rib, distance, overhang, at - - -			-	-
BEVM (3,10)	Movable sun shading device, at - - - 1., shading factor, limit value			-	-
FM (2,10)	Window dimensions, height, breadth, - - -			-	-
FORDM(2,10)	Fraction of sunlight to room air, without and with movable sun shading device			-	-
VIN (10)	Window orientation, window no.1-10			-	-
AVT (10)	Window area, - - -			-	-
TGK	Roof (horizontal) U-value•area			-	-

<u>COMMON/AD1/</u>	MAIN, ADM2, UDSKR, FRAKT	To be read or calculated in	To be used in
ITAEI(6, 30, 13)	Indexes for number of half-hours with 6 variants, 30 full degree intervals and 12 months + the whole year	ADM2	UDSKR, FRAKT
THA (50)	Temp. of accumulating layer, half-hour values	MAIN	
THO (50)	Temp. of surface, - - -	-	ADM2
THR (50)	Room air temperature - - -	-	-
SUM (11, 13)	Monthly and yearly sums	-	UDSKR
GLIM (6, 2, 13)	max. and min. temperatures, 6 variants, 12 months + the whole year	ADM2	FRAKT
<u>COMMON/INTERP/</u> MAIN, ADM2, SOLIN			
SOL (50, 2)	Solar heat through windows, delivered partly to room air, partly by radiation to surfaces. Half-hour values.	SOLIN	MAIN
SOLT (50)	Solar heat through roof and walls, half-hour values	-	-
TVIN (50)	Temperature rise of window due to absorbed sunradiation	-	-
TOO (50)	Operative temp. towards walls, -	MAIN	ADM2
TOI (50)	Operative temp. towards window and outer wall	-	-
MBA (4, 50)	Indexes for half-hours with movable sun shading device for window 1-4	SOLIN	MAIN

MAIN variables

Arrays

ELM (3) ELM(1) and ELM(3) are not used.
ELM(2) limit value for switching on or off of electric light.

IINF (366) Code 1-12, time-series number for infiltration to be used for each day during the year.

IVEN (366) Code 1-12, time-series number for ventilation to be used for each day during the year.

NBQ (4) Number of half-hours during the day, where movable sun shading device has been used for window 1-4.

ND (10) } Dates, and month, for which "big" output, with
NM (10) } half-hour values, is wanted.

QELT (50) Effect of electric lighting, when turned on.
Recorded as FLUX 10.

QKK (50) Total effect to room air, recorded through RUMDAT, i.e. exclusive electric lighting and solar radiation.

QRR (50) The same to surfaces.

QP (50) Heat conveyed to primary air for maintenance of specified minimum entry temperature, TMIT.

QOTT (12) Summation to diverse daily sums.
QOTT(1) and (2) are not used.

3 cooling load
4 heating load in the room
5 heating load in primary air
6 total heating load (4+5)
7 sun radiation
8 heat from electric lighting
9-12 not used

QTT (50) Total heating load to the room and to primary air, half-hour values.

Variables

AKL Hour for maximum room air temperature.

AT2 Summation for calculation of daily mean temperature of outer air.

AXDAG Maximum room air temperature of the day.

A1 } Coefficients for calculating the temperature of
A2 } accumulating layer. $A1 + A2 = 1$.

MAIN variables

B4	}	Coefficients for calculating the surface temperatures.
B5		
B6		
CAK	}	Fraction of heating effect supplied to room air and to surfaces. $CAK + CAR = 1$.
CAR		
CIK	}	Fraction of cooling effect supplied to room air and to surfaces. $CIK + CIR = 1$
CIR		
CKK	}	= CAK, CAR or CIK, CIR, depending on whether heating or cooling is needed.
CRR		
C1	}	Coefficients for calculating the room air temperature.
C3		
DELT		Total time during the 24 hours with max. air change, hours. (At present not printed).
DELTA		Total time during a half-hour with max. air change, hours.
DNT		= 48, number of half-hours during the day.
DT		= 0.5, time interval, not used.
I,J,J1,J2		Index in DO-loops.
ID	}	Day, month, year for the job execution. (from NEUCC library routine).
IM		
IY		
IAR		Not used.
JE	}	Is used to distinguish between full-hours and half-hours by output with half-hour values for 24 hours.
JD		
K		Index in DO-loop.
MM		Recorded as indicator for continued calculation (for MM=999).
MDG		Day-number (101-1231) for "big" output.
MEL	}	Indicator for half-hour with electric lighting or extra cooling or extra ventilation.
MVU		
NATI	}	Beginning and end of working hours, given as half-hour number + 1.
NAT		
NAP		Indicator for number of statistic outputs.
(=		-1 room air temperature only
NOP)		0 besides operative temperature
		1,2 -- besides operative temp. towards window no.1,2--
NDAG		Not used.
ND1		Not used.
NDG		Day of month, read in DISKL.
NMD		Month, - - -
NDN		Number of day of the year, 1-365, calculated in SUNR
NDT		= DNT = 48 half-hours per day.

MAIN variables

NEL	Number of half-hours during 24 hours with electric lighting.
NFLU	Number of recorded fluxes, 1-9 (excl. electric lighting, FLUX 10).
NMM	Indicator, 0 gives "small" output (one line a day), -1 suppresses the "small" output.
NINF	Not used in MAIN.
NNW	Indicator, 1 gives "big" output, 0 does not.
NOP	= NAP
NOVSK	Indicator for change of page to "small" output.
NRI NRV	} Code 1-12, indicating which time-series for infiltration or ventilation should be used for the day, which is being calculated.
NUDS	
NVEN	Number of days with "big" output, max. 10.
NVIN	Not used in MAIN.
NV=NVIN	Number of window specifications, 1-10, but max. 4, for output of status of movable sun shading device.
NVQ	Number of half-hours with extra cooling or extra ventilation.
NVU	= 2, if extra ventilation with outer air, = 4, if extra ventilation with ventilation air.
NW	NM(NW) is next day with "big" output.
PRON	Fraction of the half sphere towards the window wall occupied by wall. Used by calculation of operative temperature towards window wall.
QELK	Heat from electric lighting delivered by convection.
QELR	The same, delivered by radiation.
QLIM	Cooling load by extra cooling of the room air.
QPRIM	Heating load to primary air.
QREG	Cooling or heating load, convective share to room air.
QRMA	Greatest available heating effect, convective share to room air.
QRMI	Greatest available cooling effect, convective share to room air.
RB5	= 1./B5
RC3	= 1./C3
SLIM	Not used.
SOLLYS	Total heat of the sun through windows, also used for switching on/off electric light.
ST	Specified room data, the heat capacity of the room.

MAIN variables

SUMTHR	Summing up for calculation of the mean room air temperature of the day.
TA, TK, TO, TR	Specified room data, heat transfer factors.
TU	= TR, or $TU = TR \cdot TUU$ by window night-insulation, if any.
TUU	Reduction of total heat transfer to outer air (excl. air change) by window night-insulation.
TAKU	= TA+TK+TU
TBAS	Intermediate result for calculation of room air temperature.
THOJ	Intermediate result for calculation of surface temperature.
THOO	Highest operative temperature of the day towards walls.
THOl	In half-hour-loop: surface temperature. After CALL ADM2 : highest operative temperature of the day towards window wall.
THRl	Room air temperature.
TLIM	Highest accepted room air temperature. Above this extra cooling is delivered. Specified value.
TMIT	Lowest allowable injection temperature for primary air. Beneath this temperature is preheated. Specified value.
TNUL	Outer air temperature at 24.00 transferred to the following day at 0.00 for interpolation of the temperature at 0.30.
TOVT	Temperature increase of primary air (outer air) in fan and ductwork. Specified value.
TREG	Intermediate result, desired change of room air temperature by heating or cooling effect.
TTM	Daily mean room air temperature.
TVINJ	Intermediate result, the apparent inside temperature of the window.
TVMAX	Highest accepted room air temperature. Above this extra air-change is included, if available.
TVV	The fraction of the half-hour with max. air change for maintenance of TVMAX.
VABS	Absolute value of VVN.
VTO	Intermediate result for calculation of the coefficients B4, B5, B6, C1 and C3.
VTSUM	Total air change by ventilation and infiltration.
VVN	The difference between the normal air change and the max. possible air change (for maintenance of TVMAX).
VVV	Maximum possible air change for maintenance of TVMAX.

RUMDAT

Subroutine RUMDAT

This subroutine administrates the recording of all data concerning the room, ventilation, heat sources, movable sun shading devices and desired shape of output.

The subroutine is called ones for every calculation from MAIN. In its present form it is very confused.

Besides recording of data from type cards the subroutine controls call of the subroutine EIND which records time-series. (About type cards and time-series, see "Input Data").

Furthermore is carried out for every half-hour a summing up of heat flows (FLUXE) and a calculation of total heating and cooling effect available for the room.

At last those dates, for which "big" output is wanted, are arranged in true sequential order.

From RUMDAT the subroutine SFLUX is called, which writes out time-series of maximum heating and cooling effect and recorded heat flows.

Argument list: TA, TU, TO, TK, ST, ELM, TLIM, SLIM, TVMAX, VVV, NATI, NAT, CAK, CAR, CIK, CIR, TOVT, TMIT, NFLU, NUDS, NM, IVEN, IINF, NOP, PRON, NVIN, TUU, same names as in MAIN.

COMMON/blank/ and /SR/, Z ~ TEKST in MAIN, the remaining names are the same.

Arrays

E (1,50)	Auxiliary array for use with subroutine EIND.
ELM (3)	ELM(1) and (3) are not used. ELM(2) limit value for turning on electric lighting.
EXI (10,50)	Ten recorded fluxes, half-hour values.
IINF (366)	Code 1-12, time-series, number for infiltration to be used for each day during the year.
IVEN (366)	The same for ventilation.
MD (12)	Number of days before the first day in each month.
ND (10)	Not used.
NM (10)	Number of day (101-1231), where "big" output is wanted.
QMAS (50)	Greatest available heating effect.
QMIS (50)	Greatest available cooling effect.

Variables

A number of (3-characters) variable names correspond to 4-character strings (A-specification) for identification of input data:

AIR	AIRTemp	Air temperature, 1, 3 or 4.
ALA	LASTflux	No more data, start calculation.
ATI	A-TId	Working hours.
BEV	BEV.afsk	Movable sun shading device.
BIS	B.ISolering	Movable insulation at windows.
ELL	ELLYs	Electric illumination.
FMT	FORMat	Window height and width.
FOR	FORDel	Fraction of solar heat to room air.
FLU	FLUX	Heat flows 1-10.
HOR	HORIsont	Angle (altitude for demarcation of horizon).
INF	INFiltr	Natural air-change, infiltration.
OPE	OPERativ	Calculation of operative temperature wanted.
RIB	RIBBe	Shading effect from vertical rib or column.
QMA	QMAX	Greatest available heating effect.
QMI	QMIN	Greatest available cooling effect.
TAG	TAG	Solar heat through (flat) roof.
VAE	VAEG	Solar heat through wall.
VEN	VENT	Ventilation.
VMA	MAX-vent	Extra ventilation at high temperatures.
VND	VINDue	Window, area and orientation.
UDH	UDHAeng	Shading effect of projection over window.
UDS	UDSKriv	Control of output.

A number of variable names correspond to 2-character strings for identification of room data:

T2	TU	Room data, see description p. 9 or 31
T3	TK	- - , - - -
T4	TO	- - , - - -
T5	TA	- - , - - -
TS	S	- - , - - -
TT		Not used.
REP	blank-blank	End of room data.

Remaining variables

AVI	Internal control of infiltration or ventilation code for specified periods of the year.
BB	Recorded input value for room data.
CAK } CAR }	Fraction of total heating effect supplied by convection and radiation respectively. CAK + CAR = 1.
CIK } CIR }	Fraction of total cooling effect supplied by convection and radiation respectively. CIK + CIR = 1.
CK	Specified data, 1st parameter.
CQAK } CQAR }	Factors for convection and radiation heat respectively, for specified time-series for heating effect.
CQIK } CQIR }	The same for cooling effect.
CQQ	Factor for total heating or cooling effect in relation to specified time-series.
CR	Recorded data, 2nd parameter.
DT	= 0.5, the length of the time interval.
FEJL	Indicator for errors in input data.
FFFF	Indicator for errors in input data.
I,J,J1,J2	Indexes in DO-loops.
ID,IM,IY	Day, month, year.
I4	Not used.
KGNB } KGNS }	Starting and ending dates (day-number) for infiltration code or ventilation code.
MCK	= CK, converted to integer.
MCR	= CR, - - -
MT	Not used.
NATI } NAT }	Start and end of working hours, given as half-hour number + 1.
NB	Specified number.
NBB	= NB, but at least = 1.
NB1	= NB + 1.
NCK	= CK, converted to integer
NCR	= CR, - - -
NDT	= 48 half-hour intervals a day.
NFLU	Highest number among the recorded fluxes.
NFLX	Highest number among the recorded fluxes, apart from flux 10, electric illumination.
NJ	Index in DO-loop.
NMJ	Index used by arranging the true sequence of dates with "big" output.

NOP	Indicator for number of statistic outputs desired.
NUDS	Number of days with "big" output, max. 10.
NVEN	Highest number + 1 among the recorded ventilation time-series.
NVIN	Number of window specifications, 1-10.
N7,N8	Indexes in DO-loops.
PRON	The fraction of the half sphere towards the window wall occupied by wall. Is used by calculation of operative temperature towards window wall.
SLIM	Indicator for modification of Reference Year.
ST	Room data, heat capacity in accumulation layer.
T	Recorded name for identification of room data or input data.
TA	Room data, conductance, surface to accumulation layer.
TK	Room data, conductance, surface to neighbour room.
TLIM	Maximum accepted room air temperature, at higher temperatures extra cooling is included.
TMIT	Minimum acceptable injection temperature for primary air. Beneath this is preheated.
TO	Room data, conductance, room air to surfaces
TOVT	Temperature increase for primary air in fan and ducts.
TR	Letter 5-8 of the name on "type cards", not used.
TU	Room data, conductance, surface to outside air.
TUU	Room data, reduction of TU for movable insulation at windows.
TVMAX	Maximum accepted room air temperature. Over this extra ventilation is included.
VVV	Maximum possible air-change for maintenance of TVMAX.

Subroutine EIND

Argument list: E, MAXSUR, MAXINT, ISURF, N1,
corresponding to different variables in RUMDAT.

No COMMON's

Arrays

E(MAXSUR, MAXINT) Either E(1,48) or E(10,48).

Variables

CLOCK		Read hour from time-series card.
FLUX1	}	Values of the time-series at two hours of the day between which the half-hour values are found by linear interpolation.
FLUX2		
I		Index in DO-loop.
ISURF		The number of the flux or the air temperature, if there is more than one.
KONT		Not used.
MAXINT		= 48.
MAXSUR		Maximum dimension of the corresponding array in RUMDAT.
N1		Indicator for list output of input data.
SECINT		Number of seconds in time interval (=1800).
SECSAC		Time in seconds, for which the value in the time- series shall be calculated.
SECS1	}	Time (given in seconds) between which is interpolated.
SECS2		

This subroutine reads time-series with two or more cards and interpolates the half-hour values between the read hours.

For one time-series at least two cards are needed, at 0.00 and at 24.00 respectively, and those two cards must have the same value of function.

The subroutine is called from RUMDAT ones for every time-series which is to be read.

Subroutine SFLUX

Argument list: EXI, NFLU, NDT, QMAS, QMIS, IY, IM, ID,
NFLU ~ NFLX in RUMDAT, otherwise the same names.

COMMON/blank/, Z ~ TEKST in MAIN, otherwise the same names.

Arrays

EXI (10,50) Read fluxes, half-hour values. EXI(10,xx) is
electric lighting.
QMAS (50) Maximum heating effect, half-hour values.
QMIS (50) Maximum cooling effect, half-hour values.
NR (10) Not used.
SEXI (10) Daily sums of fluxes.
FLU (10) Headings for table.

Variables

I,N,M Indexes in DO-loops.
ID,IM,IY Day, month, year.
IT Hour for table output.
NDT = 48, numbers of intervals per 24 hours.
NFLU Numbers of read fluxes (excl. electric lighting).
M1 = 10, the number of the flux giving the electric
lighting.
TDS Number of time intervals per hour.
TI = I
TO Intermediate result for control of output.

This subroutine writes time-series with 48 half-hour values of
read FLUXes, and their daily sum, and time-series of maximum
cooling and heating effect. There are written as many FLUX as
are read, however FLUX 10 (electric illumination) and FLUX 1
are always written.

Furthermore are written time-series for the wanted room air
temperature (AIRTEMP1), the specified temperature of adjoining
room or corridor (AIRTEMP3) and of the temperature of the ven-
tilation air, if this is specified with a time-series and is not
following the temperature of the outer air.

The subroutine is called from RUMDAT once for every calculation.

DISKL, TAPL

Subroutine DISKL

Argument list: NMD, NDG, same names as in MAIN.

COMMON/KORS/, same names as in MAIN.Arrays

IA (30) Data read from disc, are converted to the different weather data.

Variables

ICA - ICK The figures 1-9, 0 and blank, are used for conversion of the cloud cover.

IAA Intermediate data in the cloud conversion.

J,K Indexes in DO-loops.

JK, KK Indexes for distribution of the concentrated data set.

NDG Day.

NMD Month.

NQ Cloud cover.

This subroutine reads the data of the Reference Year from a concentrated data set on disc store.

The data set is available as card pictures, formatted, with four hours per record ~ 80 col. punched cards. There are no missing data, except for the cloud cover, where some night hours are missing for some months.

Therefore, if the data used are given with hours 00 thru 23, either the program or the data must be adjusted.

The subroutine distinguishes between 0 and blank, i.e. missing data, for the cloud cover.

The temperatures are given with 0.1°C, radiation with 1 W/m², wind velocity with 1 knot as resolution, and the cloud cover is given with octas, i.e. 0-8, and 9 (if it has not been possible to observe the cloud cover).

The subroutine is called once for every day from MAIN.

If a concentrated dataset on disc is not available, a subroutine TAPL can read the relevant data from a complete "Test Reference Year" on tape.

Arrangement of data in the card picture:

col 1 - 3	Month-and-daynumber, 001-031, 051-078, 101-131 - etc.
col 4	1-6, six cards per day
col 5-23	Dry bulb temperature °C(I4), dewpoint temperature °C(I3), global, diffuse, and normal radiation W/m ² (3I3), cloud cover N(I1) and wind speed knots (I2).
24-42	
43-61	
62-80	

Subroutine TAPL

This subroutine reads the data of the Danish Reference Year from a tape with the original format. Corresponds generally to DISKL. One card picture per hour.

Subroutine SUNRAlgorithms

This subroutine calculates the time SO and SN for sunrise and sunset, the sun's altitude H and azimuth AS for each half-hour, and the day number DN in the year. Simplified, the longer duration of the summer half than the one of the winter half, the refraction, and the equation of the time are counted in.

DN 1 to 365. Latitude BR, -90 to 90 deg, Copenhagen 56 deg.

Calculation of the equation of time TEQ, in minutes:

$1 \leq \text{DN} < 21$	$\text{TEQ} = -2.6 - 0.44 \cdot \text{DN}$
$21 \leq \text{DN} < 136$	$\text{TEQ} = -5.2 - 9.0 \cdot \cos((\text{DN}-43) \cdot 0.0357)$
$136 \leq \text{DN} < 241$	$\text{TEQ} = -1.4 + 5.0 \cdot \cos((\text{DN}-135) \cdot 0.0449)$
$241 \leq \text{DN} < 336$	$\text{TEQ} = 6.3 + 10.0 \cdot \cos((\text{DN}-306) \cdot 0.0360)$
$336 \leq \text{DN} \leq 365$	$\text{TEQ} = -0.45 \cdot (\text{DN}-359)$

The local time, 9.7 min. (for Copenhagen), is added, and TEQ is converted into angle of time:

$\text{TET} = (\text{TEQ} - 9.7)/60.$
 $\text{TEQ} = \text{TET} \times \pi/12.$

The declination of the sun VA:

$\text{DF} = \text{DN} \cdot \pi/182.5$
 $\text{VA} = 0.33 - 22.96 \cdot \cos \text{DF} + 4.0 \cdot \sin \text{DF} - 0.37 \cdot \cos 2\text{DF} - 0.15 \cdot \cos 3\text{DF}$

Sunrise and sunset:

$\text{TON} = 12/\pi \cdot \arccos(\sin \text{BR} \cdot \sin \text{VA} + 0.0)/(\cos \text{BR} \cdot \cos \text{VA})$
 $\text{SO} = \text{TON} - \text{TET} \quad \text{sunrise}$
 $\text{SN} = 24. - \text{TON} - \text{TET} \quad \text{sunset}$

Half-hour angle, I = 1 to 48.

$\text{TP} = \text{I} \cdot \pi/24 + \text{TEQ}$

Altitude of the sun:

$\sin \text{H} = \sin \text{VA} \cdot \sin \text{BR} - \cos \text{VA} \cdot \cos \text{BR} \cdot \cos \text{TP}$

Azimuth:

$\cos \text{AS} = \text{AN} = (\sin \text{BR} \cdot \cos \text{VA} \cdot \cos \text{TP} + \cos \text{BR} \sin \text{VA})/\cos \text{H}$

Refraction (when $\text{H} > -0.005$, corresponding to about -0.3°)

$\text{H} = \text{H} + 0.000225/(\text{H} + 0.023)$

If the refraction and the longer duration of the summer half are neglected, it will give the length of the day an error of up to 12 - 13 min. at equinoxes.

SUNR

For quasi-stationary calculations, without a Test Reference Year, radiation has to be computed for the day in year, latitude, and cloud cover.

Clear sky radiation:

Optical air mass:

$$FL = 1.02 / (\sin H + 0.02)$$

Distance correction:

$$DA = 1. + 0.0334 \cdot \cos DF$$

Extinction factor EXT specified per month, see table.

Direct radiation (apparent solar constant 1163 W/m^2):

$$SM = 1163 \cdot DA \cdot e^{(-EXT \cdot FL)}$$

Diffuse radiation (empirical expression, using solar constant 1370 W/m^2):

$$HH = 0.333(1370 \cdot DA - SM) \cdot \sin H$$

Extinction factor EXT and coefficients Q and R (used below) are empirically determined values (derived from Danish data) and stored in the programme:

Month	J	F	M	A	M	J	J	A	S	O	N	D
EXT	.09	.12	.14	.16	.18	.21	.23	.23	.23	.18	.15	.11
QQR	-.039		-.0065			0		.0120		.0060	-.0390	
RRQ	-.0078		-.0121			-.0127		-.0142		-.0142	-.0078	

Radiation with cloud cover CC = 0 thru 8:

(CC = 1 corrected to 0.5, CC = 7 corrected to 7.3)

Cloud cover factor for global radiation

$$CCF = 1. + QQR \cdot CC + RRQ \cdot CC^2$$

Cloud cover factor for direct radiation:

$$CQ = 0.58 \cdot CC + 0.025 \cdot CC^3 + 0.000288 \cdot CC^5$$

Direct radiation (J = 1 thru 24)

$$RNT(J) = SM(1. - CQ/8)$$

Global radiation

$$RTOT(J) = (HH + SM \cdot \sin H) \cdot CCF$$

Diffuse radiation

$$RDT(J) = RTOT(J) - RNT(J) \cdot \sin H$$

SUNR

Argument list: NMD, NDG, NDN, same names as in MAIN

NBA2 Cloud cover, in oktas.

BA2 Date (month.day)

BAS Latitude. Default value 56° North.

COMMON/KORS/, same names as in MAIN:

Arrays

DM (12) Number of days before the first day of each month.

E (12) Extinction coefficients, per month.

RRQ (12) }
QQR (12) } Coefficient for Cloud Cover Factor calculations.

Variables

AN Solar azimuth plus π .

AZ Solar azimuth.

COSBR $\cos(\text{BR})$, latitude.

COSIH $\cos(\text{H2})$, altitude of the sun.

COSTP $\cos(\text{TP})$, hour angle.

COSVA Cosine to the declination of the sun.

DF Day number, given as angle.

DN Day number of the year, 1.-365.

H2 Altitude of the sun.

I Index in DO-loop.

NDG,NDN Day number of the year, 1 - 365.

PI = π

PJ = $\pi/180$

SINBR $\sin(\text{BR})$, latitude.

SINVA Sine to the declination of the sun.

SINUH $\sin(\text{H2})$, altitude of the sun.

TEQ, TET Equation of time

TON The half length of day, hours.

TP Hour angle.

CC = NBA2, Cloud cover, in oktas

CCF Cloud cover factor for global radiation

CQ Cloud cover factor for direct radiation

The subroutine is called from MAIN once for every day.

SOLIN

Subroutine SOLIN

This subroutine calculates solar heat through windows, roof and walls into the room.

Hereby is considered: the area and orientation of the window, any shading projection over, or ribs or columns next to the window, horizon screening (owing to other buildings or trees), furthermore transmission through the glass, dependent of angle of incidence, and movable sun shading devices considered activated when the sun radiation per sq.m. through a window exceeds a specified limit. Up to ten different windows can be included in a room.

In the Reference Year hourly values of diffuse radiation on horizontal and direct normal radiation are given, i.e. direct radiation measured on a plane perpendicular to the sun. The directional dependence of the diffuse radiation is included in the calculations and further dependent of the cloud cover.

The subroutine distributes the heat from the sun radiation to the surfaces and to the room air, generally assuming that a considerable part of the sun radiation through the window will hit curtains or lightweight objects without much heat accumulating capacity, from where the heat is very quickly transferred to the room air. If no distribution is specified, 50/50 is assumed.

The sun radiation through flat roof and walls includes the orientation of the wall and the U-value of the wall or the roof. An absorption coefficient of 0.85 and an outside heat transfer resistance of $0.05 \text{ m}^2 \text{ }^\circ\text{C/W}$ are assumed.

The time delay in wall or roof is considered simplified, as 20% of the solar heat during a half-hour is transferred immediately, and the rest is transferred, following an exponentially falling curve, decreasing 20% per half-hour.

The subroutine is called from MAIN once every day.

Algorithms

This subroutine calculates the incoming solar radiation through windows, roof, and walls to the room.

1. Transfer through roof and walls:

Outside absorption coefficient $\alpha = 0.85$
 Outside surface resistance $m_u = 0.05 \text{ m}^2 \text{ }^\circ\text{C/W}$

A delay in heat transfer is assumed, so that 20% of the transferred heat is transmitted during the first half-hour, and the rest during the following time intervals, decreasing with a factor of 0.8 per time interval. Summa = 1.0. Average delay 2 hours.

$$\text{SOLT}(I) = \text{SOLT}(I-1) \cdot 0.8$$

Transmitted during first time interval through roof:

$$\text{AT} = \text{Area} \cdot (\text{U-value}) \cdot 0.05 \cdot 0.85 \cdot 0.2 = \text{TGK} \cdot 0.0085$$

and wall IP:

$$\text{VVK} = \text{VAEK}(\text{IP}) \cdot 0.0085$$

2. Radiation on roof, $I = 2$ to 49 (the time interval).

$$\text{SOLV} = \text{SNT}(I) \cdot \sin H + \text{SDT}(I) \cdot (\sim \text{normal radiation} \cdot \sin H + \text{diffuse radiation}).$$

Transmitted through roof:

$$\text{SOLT}(I) = \text{SOLT}(I) + \text{SOLV} \cdot \text{AT}$$

3. Angle of azimuth, sun/window ($\sim$ wall):

$$X = \text{AS}(I) - \text{VIN}(\text{IP})$$

Angle of sun/window ($\sim$ wall):

$$\text{ZAN} = \cos H \cdot \cos X$$

$$\text{FV} = \text{ZAN} \text{ when } \text{ZAN} > 0, \text{ otherwise } \text{FV} = 0.$$

$$\text{VH} = \arccos(\text{ZAN})$$

4. Factor for diffuse radiation on vertical, for clear sky:

$$F = 0.55 + 0.437 \cdot \text{ZAN} + 0.313 \cdot \text{ZAN}^2.$$

$$\text{For } \text{ZAN} < -0.2: F = 0.45.$$

Correction for cloud cover, $N = 0$ to 8 ($\text{BN} = N$):

$$F = (F - 0.5) \cdot (8. - \text{BN}) / 8. + 0.5$$

Diffuse sky radiation on vertical:

$$\text{DIFD} = \text{SDT}(I) \cdot F$$

Direct radiation on vertical:

$$\text{SOLD} = \text{SNT}(I) \cdot \text{FV}$$

Reflected short-wave radiation:

$$\text{DIFR} = \text{SOLV} \cdot 0.5 \cdot 0.25$$

5. Solar heat transferred through walls and roof:

$$\text{SOLT}(I) = \Sigma (\text{SOLD} + \text{DIFD} + \text{DIFR}) \cdot \text{VVK} + \text{SOLV} \cdot \text{AT}$$

SOLIN

6. Solar heat through windows:

Calculation for stationary outside sun shading devices, if any:

$$\text{COTA} = \cos X / \tan H$$

Canopy:

$$\text{TG} = (\text{canopy protrusion}) / (\text{height of canopy over window} + \frac{1}{2} \text{ window height})$$

Fraction of the window not shaded:

$$\text{Direct: } \text{ASU} = (\text{window height} + \text{height of canopy over window} / \text{window height}) - (\text{canopy protrusion} / \text{COTA})$$

$$\text{Diffuse: } \text{ADU} = 1 / \sqrt{1 + \text{TG}^2}$$

Rib:

Fraction of the window not shaded:

$$\text{Distance of rib to window } \text{RIBA} = \text{RIBM}(1, \text{IP})$$

$$\text{ASS} = \text{protrusion of rib} \cdot \tan X$$

$$\text{Direct: } \text{ASR} = (\text{window width} + \text{RIBA} - |\text{ASS}|) / \text{window width}.$$

(Diffuse radiation is not considered reduced by vertical ribs).

Both rib and canopy:

$$\text{ASU} = \text{ASU} \cdot \text{ASR}$$

7. Factor for direct radiation transmitted through double glass window at the angle VI (0° - 90°). $\text{VI} = \text{VH} \cdot 180. / \pi$

$$\text{TR} = 0.76, \text{ transmission for } \text{VI} = 0^\circ.$$

$$\text{FK} = \text{TR} \cdot (1 - 0.04 \cdot \text{VI} / 100 - 2.933 \cdot (\text{VI} / 100)^6 + 2.13 \cdot (\text{VI} / 100)^{12})$$

Factor for transmitted diffuse radiation through double pane:

$$\text{RF} = 0.66$$

$$\text{SOLD} = \text{SOLD} \cdot \text{ASU}$$

$$\text{DIFD} = \text{DIFD} \cdot \text{ADU}$$

Through window, 1 square m:

$$\text{SOLG} = \text{SOLD} \cdot \text{FK} + (\text{DIFD} + \text{DIFR}) \cdot \text{RF}$$

8. Insertion of movable sun shading device, if $SOLG > BEVM(3,IP)$.
Solar radiation through actual window area:
 $SOLK = SOLG \cdot BEVM(1 \text{ or } 2, IP) \cdot area$,
where
 $BEVM(1, IP) = 1$, and
 $BEVM(2, IP)$ is the shading factor for the movable sun shading device.
9. Distribution of solar heat to room air:
 $SOL(I, 1) = SOLK \cdot FORD$
and to surfaces:
 $SOL(I, 2) = SOLK(1. - FORD)$
where
 $FORD$ is the distribution coefficient, normally 0.50, or as specified for the shading device.
10. Calculation of the apparent indoor overtemperature of the window, included the effect of solar heat absorbed in the glass and again given off from the glass (~no direct radiation to the sensor):
 $TVIN(I) = SOLK \cdot 0.008$
If it is desired to include direct solar radiation on the sensor, the following should be used:
 $TVIN(I) = SOLK \cdot 0.20$.

Argument list: NOP, same name as in MAIN.

COMMON/KORS/, /INTERP/ and /SR/, same names as in MAIN.

Arrays

SDT (50) Diffuse radiation on horizontal, half-hour values.
SNT (50) Direct normal radiation, half-hour values.

Variables

ADU Reduction of diffuse radiation owing to projection over the window.
ASR Reduction of direct radiation owing to ribs or columns.
ASS Horizontal shadow length of ribs.
ASU Reduction of direct radiation owing to projections over the window or ribs.
AT Intermediate result for solar heat through roof.
AV (Glass)area of window.

SOLIN

BN	Cloud cover. (0 - 8)
COSIH	$=\cos(H)$, altitude of the sun.
COTA	$=\cos(X) \cdot \cos(H) / \sin(H)$.
DIFD	Diffuse sky radiation on vertical surface.
DIFR	Reflected short wave radiation on vertical surface.
F	Direction factor for diffuse sky radiation.
FK	Transmission of direct radiation through double-pane at the angle of incidence VI.
FMB	Window width (glass).
FMH	Window height (glass).
FORD	Fraction of solar heat through windows, which goes directly to room air.
FV	$=ZAN$, during the hours from sunrise to sunset.
I,J	Indexes in DO-loops.
IA	} Counters for interpolation to half-hour values for radiation.
IB	
IP	Index in DO-loop, window specification number.
ISN	Half-hour number after sunset.
ISO	Half-hour number before sunrise.
NAF	Indicator, = 1 with movable sun shading device not activated, = 2 for activated movable sun shading device.
NOP	Indicator for calculation of the apparent indoor surface temperature of the window ($=NOP$ in MAIN).
PJ	$= \pi / 180. = 0.01745$.
RF	Transmission of diffuse radiation through double pane.
RIBA	Rib (or column), distance from nearest glass edge.
RIBF	Rib, projection in front of glass.
SOLD	Direct radiation on vertical.
SOLG	Total radiation through double pane.
SOLK	The same, with movable sun shading device, if any.
SOLV	Total radiation on horizontal.
TG	Tangent to altitude of edge of projection seen from center of pane. Is used for calculation of reduction of diffuse radiation.
TR	Transmission of direct radiation perpendicular to double pane.
UDHA	Projection, distance from upper glass edge.
UDHF	Projection, overhang in front of glass.
VH	Angle of incidence for direct radiation against pane, radian.

VI = VH, in degrees.

VVK Intermediate result for solar heat through wall.

X Solar azimuth minus azimuth angle of the windows,
roof and walls into the room.

ZAN = $\cos(H) \cdot \cos(X)$.

INPOL

Subroutine INPOL

Argument list: NULT, TOVT, TMIT.

NULT ~ TNUL in MAIN, otherwise the same names.

COMMON/KORS/, with same names as in MAIN.

COMMON/blank/, T ~ TEKST in MAIN, otherwise the same names.

No Arrays

Variables

I	Index in DO-loop.
I2 I3	} Counters for interpolation.
NULT	
TEX	Calculation of primary air temperature.
TMIT	Minimum allowable injection temperature for primary air in the room.
TOVT	Temperature increase of primary air in fan and ducts.

This subroutine converts the 24 hourly values of the outer air temperature, read from the Reference Year in subroutine DISKL (or TAPL) into 48 half-hour values. Hereby it is necessary to transfer the value at 24.00 to next day for interpolation at 0.30.

Furthermore, the temperature of the injection air (primary air) is calculated, if the air is outer air, possibly with a temperature increase TOVT from fan and ducts, and possibly with pre-heating to a minimum accepted injection temperature TMIT.

The subroutine is called from MAIN once every day.

Subroutine ADM2

Argumentlist: IM, NOP, NATI, NAT, THOO, THOl.

IM ~ NMD in MAIN, otherwise the same names.

COMMON/ADI/ and /INTERP/, same names.

No Arrays

Variables

I,J		Indexes in DO-loops.
IM		Month.
IT		Full degree interval for temperature.
NATI	} {	Start and end of working hours, given as half-hour number + 1.
NAT		
NOP		Indicator for how many operative temperatures are to be calculated (~NOP in MAIN).
THOO		Highest operative temperature of the day towards walls.
THOl		Highest operative temperature of the day towards window wall.
TI	}	Temperatures.
TJ		

In this subroutine the maximum value of operative temperature of the day towards the walls is calculated, and if NOP $\geq$ 1, of the operative temperature towards the window wall.

Furthermore is carried out sorting of the single half-hours for summing up to monthly frequencies of the respective temperatures.

The sorting is carried out both for all half-hours during the day (at 0.30 to 24.00) and for the half-hours within the working hours, NATI to NAT. (Default values: 8.30 - 17.00)

The subroutine is called from MAIN once after each day.

UDSKR

Subroutine UDSKR

This subroutine is called once from MAIN, when the calculations have been finished. It writes, monthly and for the whole year, distributions of the calculated temperatures in full degree intervals.

The distributions are written out for the air temperature, a) all day through, and b) during the working hours. Furthermore, if specified, for the operative temperature towards the walls of the room, c) all day through, and d) during the working hours, and finally e) for the operative temperature towards window and window wall during the working hours, and f) the difference between the operative temperatures towards internal walls and window plus window wall during the working hours.

a) and b) are always written out, c) and d) only if OPERativ is specified in input data, and e) and f) only if a window number, 1-10, is indicated together with OPERativ.

Together with a) is written the monthly mean value of the room air temperature, and monthly sums of cooling and heating to primary air, to the room and totally, heat from solar radiation and from electric lighting, and number of half-hours with extra cooling or extra ventilation. Analogous values are written for the year.

Together with b), d), e) and f) are calculated (in subroutine FRAKT) and written out for each month three temperatures corresponding to the quantiles 10%, 50% and 90%.

Subroutine UDSKR

Argument list: NOP, NAT, NATI, IY, IM, ID,
same names as in MAIN.

COMMON/ADI/ , with the same names as in MAIN
/blank/ Z ~ TEKST in MAIN.

Arrays

C (11) Alphameric outputs.
FRAK (3,13) Calculated temperatures corresponding to 10, 50
and 90% quantiles for 12 months and the whole year.
IS (12) Monthly number of half-hours with extra cooling.
ITOT (30) Indicator for the temperature interval to be
written. 1 ~ is written, 0 ~ is not written.
LD (6) Reduces the interval downwards.
LF (6) } Figures of first and last possible value in the
LS (6) } interval, for table headings.
NC (3) Figures 10, 50 and 90 for table headings.

Variables

ANATI } Starting and ending time for working hours,
ANAT } in hours and minutes.
I,J,K,L Indexes in DO-loops.
ID,IM,IY Day, month, year.
IRES Is used for determination of the temperature
interval to be written out.
ISUM Yearly number of half-hours with extra cooling.
JX Index in DO-loop.
LL } Indications of temperature interval to be
M } written out.
LNOP Calculates how many outputs are to be made.
NATI } Starting and ending of working hours,
NAT } given as half-hour number + 1.
NE = 11 unit in heading kWh,
= 10 - - - Mcal.
NOP Indicator for number of statistical outputs.
NN,NV,MM Indexes in DO-loops.
VARME Summing up of heat consumption, October-April.

FRAKT

Subroutine FRAKT

This subroutine calculates for every month and for the year temperatures corresponding to 10%, 50% and 90% quantiles, i.e. temperatures under which 10%, 50% and 90% of all half-hours are found.

The subroutine is called once for every calculation from UDSKR.

The calculations are carried out by cumulating the number of half-hours, selection of the full degree interval in which the quantile value must be situated, and by linear interpolation within this interval.

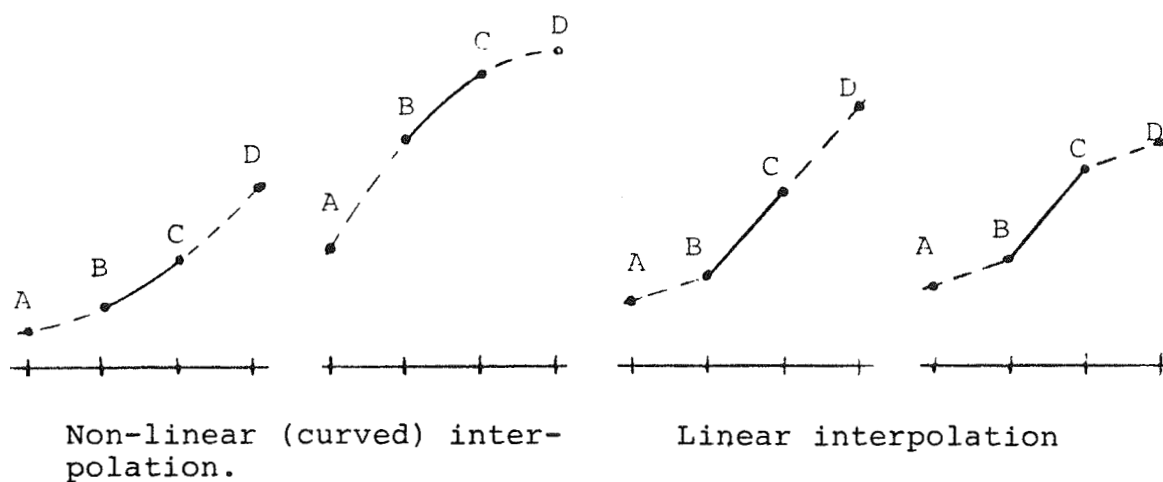
If the maximum or minimum value of the month is placed within the same interval, interpolation is not made over the entire interval, but until the extreme value only.

If the cumulated half-hour figures show a monotonous curvature over the interval and its two adjoining intervals, an interpolation is carried out after a curved line. This adjustment is scarcely significant, and may be omitted.

Algorithms

This subroutine calculates 10%, 50%, and 90% quantiles by linear or non-linear interpolation in the full degree interval in which the quantile value AN lies.

The cumulated numbers at the terminal points of the interval are B and C, and at the adjoining points A and D.



10%, 50%, or 90% of the total number (IT(30)) in the series:

$$AN = IT(30) \cdot (II \cdot 0.4 - 0.3), \quad II = 1, 2 \text{ or } 3$$

C is found when $IT(IC) > AN$, $IC = 1 \text{ to } 30$.

AM: 10-step values 0.05 to 0.95 in the interval in which interpolation shall take place.

$AM = (I - 0.5) \cdot 0.1, \quad I = 1 \text{ to } 10.$

XM: Linear interpolation in B-C.

$XM = B + AM \cdot (C - B)$

XR: Correction for non-linear interpolation in B-C.

$XR = 0.5 \cdot AM \cdot (1 - AM) \cdot (B + C - A - D).$

Non-linear interpolation is not used if $XAO = 0$, $XDO = 0$, $XR = 0$, or $XAD < 0$, i.e. for rectilinearity or S-curve.

$XAO = 2 \cdot B - D - C$

$XDO = 2 \cdot C - B - D$

$XAD = XAO/XDO$

The quantile value ANN is found for that I (and that AM), which gives XM or $XM + XR > AN$.

Subroutine FRAKT

Argument list: J, FRAK, same names as in UDSKR.

COMMON/ADI/ , same names as in UDSKR and MAIN.

Arrays

IT (30) Cumulated values of number of half-hours below a certain temperature.

FRAK (3,13) Temperatures for 10%, 50% and 90% quantiles for 12 months and the whole year.

Variables

A	Cumulated value (number) nearest under B.
AN	Limit value (number) for the quantile.
ANN	Calculated temperature for the quantile.
AM	Step by interpolation in the full degree interval.
B	Cumulated values (numbers) between which interpolation shall take place.
C	
D	Cumulated value (number) next after C.
GB	Temperatures (full degree) between which interpolation shall take place.
GC	
G6	Addend for transposition of the temperature interval.

FRAKT

I, II, M	Indexes in DO-loops.
IC	The number giving upper limit of the interval in which interpolation shall take place.
XA	Extrapolation from below.
XAD	Determination of monotonous curvature.
XAO	Deviation for final point by extrapolation from below.
XD	Extrapolation from above.
XDO	Deviation for final point by extrapolation from above.
XM	Linear interpolation.
XR	Adjustment for the curvature of the curve.
XX	Calculated value by the interpolation, calculation repeated until $XX \geq AN$.

References:

1. P. Becher: Varme og Ventilation, vol. 1 (in Danish) Teknisk Forlag 4. ed. 1971.
2. Bo Andersen et al: Meteorological Data for Design of Building and Installation: A Reference Year. (An English translation of the Danish Building Research report no. 89 about the Reference Year, Thermal Insulation Laboratory 1975.
3. Bo Andersen: TEMPFO 4. Calculation of indoor temperatures and Energy Consumption in Buildings using Climatic Data of the Reference Year (in Danish). Danish Building Research Institute, report no. 93, 1974.

FORTRAN IV G LEVEL 21

MAIN

DATE = 78125

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C THERMAL INSULATION LABORATORY, TECHNICAL UNIVERSITY, COPENHAGEN
C PROGRAM BA4 FOR CALCULATION OF ROOM TEMPERATURES
C AND HEATING AND COOLING LOADS (APRIL 78)
C FOP COPENHAGEN: LOCAL TIME= 9.7 MIN, LATITUDE= 56 DG NORTHERN
0001 COMMON /KORS/ AS(50),H(50),RNT(24),RDT(24),TT(24),FF(24),SO,SN
      1,RTOT(24),TD(24),NN(24)
0002 COMMON/SR/HORM(10),VAEK(10),UDHM(2,10),RIBM(2,10),BEVM(3,10),
      IFM(2,10),FORDM(2,10),VIN(10),AVT(10),TGK
0003 COMMON /AD1/ ITAEL(6,30,13),THA(50),THO(50),THR(50),SUM(11,13)
      1,GLIM(6,2,13)
0004 COMMON /INTERP/ SOL(50,2),SOLT(50),TVIN(50),TDO(50),TOI(50)
      1,MBA(4,50)
0005 COMMON TEKST(18), QQ(50),QK(50),QR(50),QMAX(50),QMIN(50),
      ITEX1(4,50),INFL(12,50),VENT(12,50)
0006 COMMON COK(10),COR(10),GLYS(50)
0007 DIMENSION QKK(50),QRR(50)
0008 DIMENSION IVEN(366),IINF(366)
0009 DIMENSION NM(10),ND(10)
0010 DIMENSION QP(50),QTT(50)
0011 DIMENSION QQTT(12),NBQ(4)
0012 DIMENSION QELT(50)
0013 DIMENSION ELM(3),NSLIM(20)
0014 REAL INFL
0015 DATA NSLIM / 12,14, 16,17,18,77,78,107,108,
      1335,347,348,349,354,0,0,0,0,0 /
0016 DATA SLIM / 0. /
0017 DATA NVIN / 1. /
0018 DATA BA2,BAS,NBA2 / 2*0., 0. /
0019 DATA NW,NUDS,NINF,NVEN,NM,ND / 1,0,1,1,20*0 /
0020 DATA CAK,CIK,CAR,CIR,TNUL,TOVT,TMIT,AXDAG / 2*1.,6*0. /
0021 DATA IAR,NDAG,NDT / 1, 1, 48 /
0022 DATA TVMAX,VVV,TLIM, PRON,ELM / 999.,0.,999.,4*0. /
0023 DATA TUU / 1. /
0024 DATA NOP,NATI,NAT / -1,17,34 /
0025 121 READ (5,200) TEKST
0026 200 FORMAT (18A4)

C
C INITIAL VALUES
0027 CALL DATE(ID,IM,IY)

C
C YEAR, MONTH AND DAY FOR THE RUN (NEUCC LIBRARY ROUTINE)
0028 NNM = 0
0029 NN(24) = 8
0030 NDI = NOT +1
0031 TGK = 0.
0032 SOL(1,1) = 0.
0033 SOL(1,2) = 0.
0034 SOLT(1) = 0.
0035 TNUL = 0.5
0036 DO 65 I=1,366
0037 IVEN(I)=1
0038 IINF(I)=1
0039 DO 777 J=1,50
0040 DO 780 I=1,4
0041 TEXI(I,J) = 0.
0042 780 CONTINUE
0043 DO 778 I=1,12
0044 VENT(I,J) = 0.
0045 778 INFL(I,J) = 0.
0046 QMAX(J) = 0.
0047 777 QMIN(J) = 0.
0048 DO 779 I=1,10
0049 VIN(I) = 0.
0050 AVT(I) = 0.
0051 HORM(I) = 1.
0052 VAEK(I) = 0.
0053 DO 776 J=1,2
0054 FORDM(J,I) = 0.5
0055 UDHM(J,I) = 0.
0056 RIBM(J,I) = 0.
0057 776 FM(J,I) = 0.
0058 BEVM(1,I) = 1.
0059 BEVM(2,I) = 1.
0060 BEVM(3,I) = 999.
0061 COK(I) = 1.
0062 779 COR(I) = 0.
0063 NFLU = 1
0064 DT = 0.5
0065 SLIM = 0.
0066 NNW = 0
0067 926 CONTINUE
0068 18 WRITE (6,111) TEKST,IY,IM,10
0069 111 FORMAT (1H1,18A4,4H 19,12,3H - ,12,3H - ,12 )
0070 WRITE (6,113)
0071 113 FORMAT (1H0,25X,'THERMAL INSULATION LAB., DANISH TECHNICAL UNIVERS
      1ITY',26X,'PROGFAM BA4, VERSION APRIL 1977')

C
C READING DATA FOR THE ROOM AND EXITATIONS, AND OUTPUT SPECIFICATIONS
0072 CALL RUMDAT(TA,TU,TO,TK,ST,ELM,TLIM,SLIM,TVMAX,VVV,NATI,NAT,
      1CAK,CAR,CIK,CIF,TOVT,TMIT,NFLU,NUDS,NM,IVEN,IINF,NOP,PRON,NVIN,
      2TUU,BA2,BAS,NBA2 )
0073 NW=1
0074 IF (NM(10).EQ.-1) NNM=1
0075 NM(10) = 0
0076 NSL = 1
0077 TR = TU
0078 NV = NVIN
0079 IF (NV.GT.4) NV = 4
0080 NAP = NOP
0081 IF (NAP.LE.0) NAP = 99
0082 THR(49) = TEXI(1,1)
0083 THO(49) = TEXI(1,1)
0084 THA(49) = TEXI(1,1)
0085 SOLT(49) = 0.
0086 QQ(49) = 0.
0087 DO 52 J1=1,NDT
0088 QKK(J1) = QK(J1)
0089 QRR(J1) = QR(J1)

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0090      52 CONTINUE
0091      DO 2 I=1,13
0092      DO 3 J=1,11
0093      3 SUM(J,1) = 0.
0094      DO 9 J=1,6
0095      GLIM(J,1,1) = 100.
0096      GLIM(J,2,1) = -100.
0097      DO 9 K=1,30
0098      9 ITAEL(J,K,1) = 0.
0099      2 CONTINUE

C
C COEFFICIENT TO TEMPERATURE OF THE HEAT ACCUMULATING LAYER
0100      A2=TA*0.5/ST
0101      A1=1.-A2
0102      NMD =BA2
0103      NDG = (BA2 -FLOAT(NMD))*100.01
0104      5 CONTINUE
0105      IF (BA2.NE.0.) GOTO 345

C
C READING WEATHER DATA FOR ONE DAY (24 HOURS)
0106      CALL TAPL(NMD,NDG)
C      CALL DISKL(NMD,NDG)

C
C CALCULATING HEIGHT AND AZIMUT OF SUN AND RADIATION IF BA2 IS SPECI-
C FIED
0107      345 CALL SUNR(NMD,NDG,NDN,NBA2,BA2,BAS)

C
C REDUCTION OF THE NORMAL RADIATION IN DECEMBER, JANUARY, MARCH AND
C APRIL IF SLIM=1 I.E. IF MODREF IS SPECIFIED
0108      IF (NDN.NE.NSLIM(NSL).OR.SLIM.NE.1.) GOTO 939
0109      NSL=NSL+1
0110      DO 938 I=1,24
0111      938 RNT(I) = 0.
0112      939 CONTINUE

C
C SOLAR RADIATION ON WALLS AND ROOF, AND THROUGH WINDOWS, WITH SHADING
0113      CALL SOLIN(NDP)

C
C HALF-HOUR VALUES OF TEMPERATURES IN OUTDOOR AIR AND VENTILATION
C (PRIMARY) AIR
C HALVTIMESVAERDIER AF TEMPERATURE I UDELUFT OG PRIMAERLUFT
0114      CALL INPOL(TNUL,TOVT,TMIT,BA2)
0115      NRV = IVEN(NDN)
0116      NRI = IINF(NDN)
0117      LBA2 = 0
0118      436 CONTINUE
0119      IF (BA2.NE.0.) LBA2 =LBA2 +1
0120      NVQ = 0
0121      NEL = 0
0122      DO 838 K=1,4
0123      838 NBQ(K) = 0
0124      THA(1) = THA(NDT+1)
0125      THO(1) = THO(NDT+1)
0126      THR(1) = THR(NDT+1)
0127      QO(1) = QO(NDT+1)
0128      DO 388 J=1,12
0129      388 QQT(J) = 0.
0130      SUMTHR = 0.
0131      AT2 = 0.
0132      AXDAG=0.
0133      DELT = 0.
0134      NOVSK =NDN - (NDN /61)*61
0135      MDG = 100*NMD +NDG +LBA2
0136      IF (MDG.EQ.NM(NW).OR.LBA2.EQ.1.OR.LBA2.EQ.10) GOTO 921
0137      GO TO 950
0138      921 NW =NW +1
0139      NNW =1
0140      WRITE (6,111) TEKST,IY,IM,ID
0141      IF (SLIM.EQ.1.) WRITE (6,81)
0142      81 FORMAT (' MODIFIED REFERENCE YEAR USED ')
0143      WRITE (6,112) NMD,NDG,NAP,(K,K=1,NV)
0144      112 FORMAT ('HOMONTH ',12,7H DAY ',12,7H KL RL-T OP-T OPT',
0145      111,2X,
0146      11 UDLT QREG QPRIM QTOT SOLIND UVQ E-L B-A',11,12,213/)

0145      750 CONTINUE

C
C START OF HALF-HOUR LOOP
0146      66 DO 50 J2= 1,NDT
0147      J1=J2
0148      J=J2+1
0149      MVU = 0
0150      MEL = 0
0151      TU =TR
0152      QLIM = 0.
0153      SOLLYS =SOL(J,1) +SOL(J,2)

C
C NIGHT-INSULATION, IF ANY
0154      IF (J2.GT.14.AND.J2.LT.36) GOTO 765
0155      IF (NDN.LT.100.OR.NDN.GT.300) TU =TR*UUU
0156      765 CONTINUE
0157      TAKU=TA+TK+TU
0158      VTSUM = VENT(NRV,J1) +INFL(NRI,J1)
0159      VTO =1. +VTSUM/TO

C
C COEFFICIENTS TO ROOM-AIR TEMPERATURE
0160      C1 =1./VTO
0161      RC3 =TO +VTSUM
0162      C3 = 1./RC3

C
C COEFFICIENTS TO SURFACE TEMPERATURE
0163      B1=B6*TA, B2=B6*TK, B3=B6*TU,
0164      B5 =1./((TAKU*VTO +VTSUM)
0165      B4 =B5*VENT(NRV,J1)
0166      B6 =B5*VTO
0167      RB5 =TAKU *VTO +VTSUM
0168      QELT(J) = 0.
0169      QK(J2) =QKK(J2) +SOL(J,1)
0170      QR(J2) =QRR(J2) +SOL(J,2) +SOLT(J)
0171      QQT(7) =QQT(7) +SOLLYS +SOLT(J)

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C
C SWITCHING ELECTRIC LIGHT, IF ANY (FLUX 10)
0171 IF (SOLLYS.GE.ELM(2)) GOTO 399
0172 IF (OLYS(J2).LE.0.) GOTO 399
0173 QELK = OLYS(J2)*CDK(10)
0174 QELR = OLYS(J2)*CDR(10)
0175 QK(J2) = QK(J2) + QELK
0176 QR(J2) = QR(J2) + QELR
0177 QQTT(8) = QQTT(8) + QELR + QELK
0178 QELT(J) = QELK + QELR
0179 MEL = 1
0180 399 CONTINUE
0181 AT2 = AT2 + TEXI(2,J2)

C
C CALCULATION OF TEMPERATURES WITHOUT COOLING OR HEATING
0182 THA(J) = THA(J2)*A1 + THO(J2)*A2
0183 THOJ = THA(J)*B6*TA + TEXI(2,J2)*B6*TA + TEXI(3,J2)*B6*TK
      1 + TEXI(4,J2)*B6 + QK(J2)*B5 + QR(J2)*B6
      2 + TEXI(2,J2)*B5*INFL(NRI,J2)
0184 TBAS = TEXI(2,J2)*C3*INFL(NRI,J2) + TEXI(4,J2)*C3*VENT(NRV,J2)
      1 + QK(J2)*C1/TO
0185 TREG = TEXI(1,J2) - TBAS - THOJ*C1

C
C REGULATION EFFECT (COOLING OR HEATING)
0186 QREG = TREG*TO/C1
0187 QDMA = QMAX(J2)*CAK
0188 QDMI = QMIN(J2)*CIK
0189 CRR = CAR
0190 IF (QREG.LT.0.) CRR = CIR
0191 CKK = 1. - CRR
0192 QREG = QREG/(1. + (B6*CRR/CKK + B5)*TO)
0193 QQ(J) = QREG/CKK
0194 IF (QREG.LT.QDMI) QQ(J) = QMIN(J2)
0195 IF (QREG.GT.QDMA) QQ(J) = QMAX(J2)
0196 THO(J) = THOJ + QQ(J)*(CRR*B6 + CKK*B5)
0197 THR(J) = TBAS + THO(J)*C1 + QQ(J)*CKK*C1/TO
0198 IF (QREG.LT.0.) QTT(3) = QTT(3) + QQ(J)
0199 IF (QREG.GT.0.) QTT(4) = QTT(4) + QQ(J)

C
C TEMPERATURE LIMITATION THROUGH ADDITIONAL COOLING OF ROOM AIR
0200 IF (THR(J).LE.TLIM) GOTO 525
0201 TREG = TLIM - THR(J)
0202 QLIM = TREG*TO/(C1 + B5*TO)
0203 THO(J) = THO(J) + QLIM*B5
0204 THR(J) = THR(J) + QLIM*(C3 + B5*C1)
0205 QTT(3) = QTT(3) + QLIM
0206 QQ(J) = QLIM
0207 SUM(9,NMD) = SUM(9,NMD) + 1.
0208 MVU = 1
0209 525 CONTINUE
0210 THR1 = THR(J)
0211 THO1 = THO(J)

C
C TEMPERATURE LIMITATION BY INCREASED VENTILATION, CALCULATED AFTER
C COOLING, IF ANY.
0212 IF (THR(J).LE.TVMAX) GOTO 526

C
C NVU=2 INCREASE WITH OUTSIDE AIR, NVU=4 INCREASE WITH VENTILATION AIR
0213 NVU = 2

C
C INCREASED AIRCHANGE, ONLY IF IT GIVES LOWER ROOM TEMPERATURE
0214 IF (THR(J).LT.TEXI(NVU,J2)) GOTO 526
0215 DELTA = 0.5
0216 VVN = VVV - VENT(NRV,J2)
0217 TVV = VVN
0218 IF (VVN.LT.0.1) GOTO 526
0219 THR1 = (THR(J)*RC3 + TEXI(NVU,J2)*VVN)/(RC3 + VVN)

C
C (INFLUENCE ON THO1 NEGLECTED)
0220 IF (THR1.GE.TVMAX) GOTO 527

C
C INCREASE OF AIRCHANGE ONLY UNTIL TVMAX IS REACHED
0221 TVV = (THR(J) - TVMAX)*RC3/(TVMAX - TEXI(NVU,J2))
0222 DELTA = 0.5*TVV/VVN
0223 THR1 = TVMAX
0224 527 THR(J) = THR1
0225 VTSUM = VTSUM + TVV
0226 VTO = 1. + VTSUM/TO
0227 B5 = 1./(TAKU*VTO + VTSUM)
0228 B6 = B5*VTO
0229 THO1 = (THA(J)*TA + TEXI(2,J2)*TA + TEXI(3,J2)*TK + QR(J2)*B6
      1 + QQ(J)*(CRR*B6 + CKK*B5) + QLIM*B5
      2 + (TEXI(4,J2)*VENT(NRV,J2) + TEXI(2,J2)*INFL(NRI,J2) + QK(J2)*B5
      3 + TEXI(NVU,J2)*TVV*B5
      THO(J) = THO1

C
C COUNTING HOURS WITH MAX. AIRCHANGE
0231 DELT = DELT + DELTA
0232 MVU = 1
0233 526 CONTINUE
0234 QPRIM = (TEXI(4,J2) - TEXI(2,J2) - TOVT)*VENT(NRV,J2)
0235 QTT(J) = QPRIM
0236 QQ(J) = QPRIM
0237 IF (QQ(J).GT.0.) QTT(J) = QTT(J) + QQ(J)
0238 QTT(5) = QTT(5) + QPRIM

C
C TEMPERATURE OF INSIDE SURFACE OF WINDOW AND WALL
0239 TVINJ = TVIN(J) + (THR(J) + THO(J))/3.2 + TEXI(2,J2)*0.375
0240 TOI(J) = (THR1 + THO1)/2.
0241 TOI(J) = (THR1 + TVINJ*(1.-PRON) + THO(J)*PRON)/2
0242 SUMTHR = SUMTHR + THR1
0243 IF (AXDAG.GE.THR1) GOTO 901
0244 AXDAG = THR1
0245 AKL = FLOAT(J2 - (J2/2)*2)*0.3 + FLOAT(J2/2)
0246 901 CONTINUE

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C
C  NUMBER OF HALF-HOURS WITH ADDITIONAL COOLING, INCREASED VENTILATION,
C  ELECTRIC LIGHT OR MOVABLE SUNSHADING FOR WINDOW NO 1 -4
0247   NVQ =NVQ +MVU
0248   NEL =NEL +MEL
0249   DO 837 K=1,NV
0250   837 NBQ(K) =NBQ(K) +MBA(K,J)
0251   IF (NNW.E2.0) GOTO 50
0252   JD =J1/2
0253   JE =J/2

C
C  PRINTOUT OF HALF-HOUR VALUES FOR AN ENTIRE DAY
0254   IF (JE.NE.JD) GOTO 444
0255   WRITE (6,953) JD,THR1,TD0(J),TD1(J),TEXI(2,J2),QQ(J),QP(J),
      1 QTT(J),SOLLYS,MVU,MEL,(MBA(K,J),K=1,NV)
0256   953 FORMAT (1H,13,4F7.1,4F8.1,3I5,3I3 )
0257   IF (J2.EQ.0) NNW=0
0258   NOVSK =1
0259   GO TO 50
0260   444 WRITE (6,954)   THR1,TD0(J),TD1(J),TEXI(2,J2),QQ(J),QP(J),
      1 QTT(J),SOLLYS,MVU,MEL,(MBA(K,J),K=1,NV)
0261   954 FORMAT (1H,3X,4F7.1,4F8.1,3I5,3I3 )
0262   50 CONTINUE

C
C  END OF HALF-HOUR LOOP
0263   IF (NOVSK.NE.1) GOTO 955
0264   956 NNW =0
0265   IF (NMM.EQ.1) GOTO 955
0266   WRITE (6,111) TEKST,IY,IM,ID
0267   913 FORMAT (1H1)
0268   WRITE (6,912) NAP,(I,I=1,NV)
0269   912 FORMAT (1H,1MD DG RLT M KL FLT MAX DP-T OPT',I1,' UDT M',
      1 ' Q KOLE Q VAPM Q PRIM Q SOL UVQ E-L B-A',I1,3I4)
0270   955 CONTINUE

C
C  DISTRIBUTING AND COUNTING VALUES FOR MONTHLY AND YEARLY TABLES
0271   CALL ADM2(NMD,NOP,NAT1,NAT,TH00,TH01)
0272   DNT =DNT
0273   TTM =SUMTHR/DNT
0274   AT2 =AT2/DNT
0275   DO 389 J=3,8
0276   389 QQTT(J) =QQTT(J)*DT
0277   QQTT(6) =QQTT(4) +QQTT(5)
0278   SUM(1,NMD) =SUM(1,NMD) +TTM
0279   DO 390 J=2,7
0280   390 SUM(J,NMD) =SUM(J,NMD) +QQTT(J+1)
0281   SUM(11,NMD) =SUM(11,NMD) +1.
0282   IF (NMM.EQ.1) GOTO 982

C
C  PRINTOUT OF LINE OF DAILY VALUES
0283   WRITE (6,902) NMD,NDG,TTM,AKL,AXDAG,TH00,TH01,AT2,(QQTT(J),J=3,5),
      1 QQTT(7),NVQ,NEL,(NBQ(I),I=1,NV)
0284   902 FORMAT (1H,12,13, F7.1,F8.2,F5.1,3F7.1,4F9.0,3I6,3I4)
0285   IF (DELT.NE.0.) WRITE (6,528) DELT
0286   528 FORMAT (1H,F5.1)
0287   982 CONTINUE
0288   IF (LBA2.GT.0.AND.LBA2.LT.10) GOTO 436
0289   IF (BA2.NE.0.) GOTO 985
0290   IF (NMD.NE.12.OR.NDG.NE.31) GOTO 5

C
C  TERMINATION AND PRINTOUT AFTER DECEMBER 31.
0291   CALL UDSKR(NOP,NAT,NAT1,IY,IM,ID,SLIM)
0292   985 CONTINUE
0293   READ (5,925) MM
0294   925 FORMAT (I3)
0295   IF (MM.NE.999) STOP

C
C  NEW CALCULATION IF MM=999, OTHERWISE STOP
0296   REWIND 1
0297   GOTO 926
0298   END

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0001   SUBROUTINE EIND(E,MAXSUR,MAXINT,ISURF,N1)
C  READ TIME-DEPENDANT VARIABLES, GENERATE TIME-SERIES, 48 HALF-HOURS
0002   DIMENSION E(MAXSUR,MAXINT)
0003   IF (N1.EQ.2) WRITE(6,31)
0004   31 FORMAT (1H)
0005   SECINT=24*60*60/MAXINT
0006   COUNT=1
0007   SECS2=-99999999
0008   DO 10 I=1,MAXINT
0009   SECSAC=FLOAT(I)*SECINT
0010   IF (SECSAC.EQ. SECS2) GO TO 20
0011   19 CONTINUE
0012   SECS1=SEC
0013   FLUX1=FLUX
0014   READ(5,10) CLOCK,FLUX2
0015   100 FORMAT (1H,2,5X,F10.2)
0016   IF (N1.EQ.2) WRITE(6,10) CLOCK,FLUX2
0017   30 FORMAT (1H,2,5X,F10.2)
0018   SECS2=FLUX2*(CLOCK-1)*FIX(CLOCK)+FIX(CLOCK)
0019   IF (SECSAC.GT. SECS2) GO TO 19
0020   20 CONTINUE
0021   E(ISURF,I)=FLUX1 + (FLUX2-FLUX1)*(SECSAC-SECS1)/(SECS2-SECS1)
0022   10 CONTINUE
0023   RETURN
0024   END

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0001 SUBROUTINE RUMDAT(TA,TU,TO,TK,ST,ELM,TLM,SLIM,TVMAX,VVV,NATI,NAT,
      1CAK,CAR,CIK,CIR,TOVT,TMIT,NFLU,NUDS,NM,IVEN,IINF,NOP,PRON,NVIN,
      2TUU,BA2,BAS,NBA2 )
C   READING FROM CARDS CONSTANTS FOR THE ROOM (TU, TO, TK, TA AND S)
C   HEATFLUXES AS TIMESERIES (FLUX)
C   AVAILABLE HEATING- AND COOLING EFFECT (QMAX AND QMIN) FOR
C   KEEPING THE DESIRED TEMPERATURE (AIRTEMP 1)
C   DISTRIBUTION OF FLUX, QMAX AND QMIN ON RADIATION -CONVECTION
C   TEMPERATURE IN ADJACENT ROOMS AND OF VENTILATION AIR
C   (AIRTEMP 3 AND 4)
C   VENTILATION AND INFILTRATION (VENT AND INFILT)
C   WINDOW AREAS AND ORIENTATIONS (VINDUE)
C   FIXED, OUTSIDE SUNSHADINGS, CANOPIES, RIBS (UDHAENG, RIBBE)
C   MOVABLE SUNSHADINGS, SETVALUES AND SHADING FACTOR (BEV,AFSK)
C   MOVABLE NIGHT INSULATION, E.G. AT THE WINDOW (B.ISOL)
C   ALTITUDE OF HORIZON, DEGREES (HORIZON)
C   SETVALUE OF TEMPERATURE FOR INCREASED VENTILATION OR COOLING
C   ELECTRIC LIGHT, POWER AND SETVALUE FOR SWITCHING (ELLYS)
C   ROOF AND WALLS WITH SUN, AREAS AND U-VALUES (TAG OG VAEG)
C   WORKING HOURS (A-TID)
C   SPECIFICATION OF DESIRED OR SUPPRESSED OUTPUT
C   THIS SUBROUTINE IS A VERY CLUMSY PATCHWORK

0002 COMMON Z(18), QQ(50), QK(50), QR(50), QMAX(50), QMIN(50),
      1TEXI(4,50), INFL(12,50), VENT(12,50)
0003 COMMON COK(10), COR(10), QLYS(50)
0004 COMMON SR/HDRM(10), VAEK(10), UDHM(2,10), PIBM(2,10), BEVM(3,10),
      1RM(2,10), FORDM(2,10), VIN(10), AVT(10), TKG
0005 DIMENSION NM(10), ND(10), ELM(3)
0006 DIMENSION QMAS(50), QMIS(50)
0007 DIMENSION EXI(10,50), E(1,50)
0008 DIMENSION IVEN(366), IINF(366), MD(12)
0009 INTEGER FEJL
0010 REAL INFL, INF
0011 DATA AIR, FLU, QMA, QMI, VEN/4HAIRT, 4HFLUX, 4HQMAX, 4HQMIN, 4HVENT /
0012 DATA INF, UDS, HOR, VAE, UDH, RIB, BEV, ELL, FOP / 4HINFI, 4HUDSK, 4HHORI,
      14HVAEG, 4HUDHA, 4HRIBB, 4HBEV, 4HELLY, 4HFORD /
0013 DATA CQAK, CQAF, CQIK, CQIR /1.0,1.0,1.0,1.0 /
0014 DATA REFMO / 4HMODF /
0015 DATA BIS, BAA / 4HB, IS, 4FBA2 /
0016 DATA VND, TAG, ALA / 4HVIND, 4HTAG, 4HLAST /
0017 DATA REP, T2, T3, T4, T5, TS, TT / 2H, 2HTU, 2HTK, 2HTO, 2HTA, 2HS, 2HDT /
0018 DATA INF, FMT, VMA, ATI, OPE / 4HINFI, 4HFORM, 4HMAX-, 4HA-TI, 4HOPR /
0019 DATA MD / 0.31, 59.90, 120.151, 181.212, 243.273, 304.334 /
0020 DATA NFLX / 0 /
0021 DATA QMAS, QMIS, EXI / 600*0. /
0022 FFFF = 1
0023 NDT = 48
0024 DT = 0.5
0025 FEJL = 1
0026 21 READ (5,101) T,BB
0027 101 FORMAT (A2,F10.2)
0028 MT = 1
0029 J4 = 1

C   FDP A FURTHER CALCULATION IN THE SAME ROOM A BLANK CARD ONLY INDICA-
C   TES NO CHANGES IN THE ROOM CONSTANTS
C   FDP A FURTHER CALCULATION WITH THE SAME EXITATIONS ETC A "LASTFLUX"
C   CARD ONLY INDICATES NO CHANGES

0030 11 IF (T.NE.T2) GOTO 12
0031 TU=BB
0032 GO TO 21
0033 12 IF (T.NE.T3) GOTO 13
0034 TK=BB
0035 GO TO 21
0036 13 IF (T.NE.T4) GOTO 14
0037 TO=BB
0038 GO TO 21
0039 14 IF (T.NE.T5) GOTO 15
0040 TA=BB
0041 GO TO 21
0042 15 IF (T.NE.TS) GOTO 16
0043 ST=BB
0044 GO TO 21
0045 16 CONTINUE
0046 17 IF (T.EQ.REP) GOTO 18
0047 19 WRITE (6,112)
0048 112 FORMAT(1H0,'INPUTERROR, WRONG T-CODE, OR S AND TO CANNOT BE ZERO')
0049 FEJL = 2
0050 GO TO 21
0051 18 CONTINUE
0052 WRITE (6,102) TU,TK,TO,TA,ST,DT
0053 102 FORMAT (1H0, 4HTU =,F10.2, 5X,4HTK =,F10.2, 5X,4HTO =,F10.2,
      15X,4HTA =,F10.2/1X,4HS =,F10.2,5X,4HDT =,F10.2 )
0054 IF (FEJL.GT.1.1) STOP
0055 IF (TO.LE.0.) GOTO 19
0056 IF (ST.LE.0.) GOTO 19
0057 IF ((TA+TK+TU).LE.0.) GOTO 19
0058 41 READ (5,703) T,TR,NB,CK,CR
0059 709 WRITE (6,104) T,TR,NB,CK,CR
0060 104 FORMAT (1H0,2A4,I2,2F10.3 )
0061 703 FORMAT (2A4,I3,2F10.3)
0062 AVI = 2
0063 NBI =NB +1
0064 NBR =NB
0065 IF (NBB.LE.0) NBB=1
0066 FEJL = 1
0067 IF (T.EQ.ALA) GOTO 43
0068 IF (T.EQ.REFMO) GOTO 400
0069 IF (NB.LT.0) FEJL=3
0070 IF (T.EQ.MI.AND.NB.GE.0) GOTO 401
0071 IF (NB.GT.10) FEJL = 3
0072 IF (T.EQ.VMA) GOTO 491
0073 IF (T.EQ.ATI) GOTO 492
0074 IF (T.EQ.OPE) GOTO 493
0075 IF (T.EQ.BAA) GOTO 1414
0076 IF (T.EQ.HOP) GOTO 1431
0077 IF (T.EQ.UDH) GOTO 1433

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0073      IF (T.EQ.218) GOTO 434
0079      IF (T.EQ.FOR) GOTO 437
0080      IF (T.EQ.315) GOTO 467
0081      IF (NB.LE.12) FEJL=1
0082      401 IF (CK.EQ.0..AND.CR.EQ.0.) GOTO 774
0083      IF (T.EQ.QMI) GOTO 404
0084      IF (T.EQ.INF.AND.NB.LE.12) GOTO 406
0085      IF (T.EQ.VEN.AND.NB.LE.12) GOTO 407
0086      IF (NB.GT.10) FEJL=3
0087      IF (T.EQ.UDS) GOTO 405
0088      IF (T.EQ.TAG) GOTO 402
0089      IF (T.EQ.QMA) GOTO 403
0090      IF (T.EQ.ELL) GOTO 436
0091      IF (T.EQ.VAE) GOTO 432
0092      IF (T.EQ.BEV) GOTO 435
0093      IF (T.EQ.FMT) GOTO 438
0094      IF (NB.LT.1) FEJL=3
0095      IF (T.EQ.VND) GOTO 408
0096      IF (T.EQ.FLU) GOTO 409
0097      IF (T.EQ.AIR) GOTO 410
0098      FEJL=22
0099      774 CONTINUE
0100      IF (T.EQ.QMA) GOTO 421
0101      IF (T.EQ.QMI) GOTO 422
0102      IF (T.EQ.INF) GOTO 423
0103      IF (T.EQ.VEN) GOTO 424
0104      IF (NB.LT.1.OR.NB.GT.10) FEJL=3
0105      IF (T.EQ.FLU) GOTO 425
0106      IF (T.EQ.AIF) GOTO 426
0107      FEJL=2
0108      GO TO 418
0109      467 TUU=CK
0110      GOTO 418
0111      481 TVMAX=CK
0112      VVV=CR
0113      GO TO 418
0114      482 NCK= IFIX(CK)
0115      NATI=NCK*2+IFIX((CK-FLOAT(NCK)+0.001)/0.6)
0116      NCR= IFIX(CR)
0117      NAT=NCR*2+IFIX((CR-FLOAT(NCR)+0.001)/0.6)
0118      GO TO 418
0119      483 NOP=NB
0120      PRON=CK
0121      GO TO 418
0122      400 SLIM=1.
0123      GO TO 418
0124      402 TGK=CR*CK
0125      GO TO 418
0126      403 CQAK=CK
0127      CQAR=CR
0128      GO TO 411
0129      404 CQIK=CK
0130      CQIR=CR
0131      IF (NB.GT.0) TLIM=NB
0132      411 IF (CK.LE.0..AND.CR.GT.0.) WRITE (6,117)
0133      GO TO 418
0134      117 FORMAT (1H0,'INPUT ERROR, QMAX AND QMIN MUST DELIVER SOME PART OF',
0135      1 ' THE EFFECT CONVECTIVELY')
0136      405 IF (CK.LT.0..OR.CK.LT.0.) NM(10)=-1
0137      IF (CK.LE.0.) GOTO 451
0138      NUOS=NUOS+1
0139      IF (NUOS.GT.10) GOTO 418
0140      NM(NUOS)=CK*100.001
0141      451 IF (CR.LE.0.) GOTO 418
0142      NUOS=NUOS+1
0143      IF (NUOS.GT.10) GOTO 418
0144      NM(NUOS)=CR*100.001
0145      GO TO 418
0146      1414 BA2=CK
0147      BAS=CR
0148      NBA2=NB
0149      C PA2-SPECIFICATION MUST PRECEED THE AIRTEMP 2 SPECIFICATION
0150      C BA2 DAY FOR SUN-CALCULATION, BAS LATITUDE, NBA2 CLOUD COVER 0 - 8
0151      GO TO 41
0152      406 IF (NB.LE.NINF) GOTO 412
0153      WRITE (6,114)
0154      114 FORMAT (1H0,'WRONG TIMESERIES SPECIFIED FOR VENT. OR INFILTR.')
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RUMDAT

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0182      1433 UDHM(1,NBB) =CK
0183      UDHM(2,NBB) =CR
0184      GO TO 418
0185      434 RIBM(1,NBB) =CK
0186      RIBM(2,NBB) =CR
0187      GO TO 418
0188      435 BEVM(3,NBB) =CK
0189      BEVM(2,NBB) =CP
0190      GO TO 418
0191      436 ELM(2) =CK
0192      GO TO 418
0193      437 FORDM(1,NBB) =CK
0194      FORDM(2,NBB) =CR
0195      GO TO 418
0196      438 FM(1,NBB) =CK
0197      FM(2,NBB) =CR
0198      GO TO 418
0199      421 CALL EIND(QMAS,1,NDT,1,1)
0200      GOTO 418
0201      422 CALL EIND(QMIS,1,NDT,1,1)
0202      IF (NB.GT.0) TLIM =NB
0203      GO TO 418
0204      423 IF (NINF.LT.NB1) NINF=NB1
0205      CALL EIND(E,1,NDT,1,2)
0206      DO 431 J=1,NDT
0207      431 INFL(NB1,J) =E(1,J)
0208      GO TO 418
0209      424 IF (NVEN.LT.NB1) NVEN=NB1
0210      CALL EIND(E,1,NDT,1,2)
0211      DO 433 J =1,NDT
0212      433 VENT(NB1,J) =E(1,J)
0213      GO TO 418
0214      425 IF (NB.GT.NFLU) NFLU=NB
0215      IF (NB.NE.10.AND.NB.GT.NFLX) NFLX =NB
0216      CALL EIND(EXI,10,NDT,NB,1)
0217      GO TO 418
0218      426 IF (NB.EQ.10) NB=4
0219      IF (NB.GT.4) FEJL =3
0220      IF (NB.EQ.2.AND.BA2.EQ.0.) FEJL =3
0221      IF (NB.EQ.4) TMIT =0.
0222      IF (NB.EQ.4) TOVT =0.
0223      CALL EIND(E,1,NDT,1,1)
0224      DO 427 J=1,NDT
0225      427 TEXI(NB,J) =E(1,J)
0226      418 IF (FEJL.EQ.1) GOTO 41
0227      WRITE (6,965) FEJL
0228      965 FORMAT (1H ,76)
0229      FFFF =2
0230      IF (FEJL.NE.3) GOTO 621
0231      WRITE (6,108)
0232      GO TO 41
0233      621 WRITE (6,113)
0234      108 FORMAT (1H0,'INPUTERROR, INVALID NUMBER' )
0235      113 FORMAT (1H0,'INPUTERROR, WRONG EXITATION CODE ' )
0236      GO TO 41
0237      43 IF (FFFF.EQ.2) GO TO 300

C
C   CRONOLOGISATION OF SPECIFIED DAYS WITH "BIG" LIST OUTPUT
0238      DO 958 I=1,9
0239      DO 957 J=1,9
0240      IF (BA2.NE.0.) NM(I)= BA2
0241      IF (NM(J+1).EQ.0) GOTO 958
0242      IF (NM(J).LE.NM(J+1)) GOTO 957
0243      NMJ =NM(J)
0244      NM(J) =NM(J+1)
0245      NM(J+1) =NMJ
0246      957 CONTINUE
0247      958 CONTINUE

C
C   CALCULATION OF TOTAL HEAT FLUX EXCL. ELECTRIC LIGHT AND
C   POSSIBLE VENTILATION AIR
0248      DO 48 J1=1,NDT
0249      IF (TMIT.NE.0.) TEXI(4,J1) =0.
0250      IF (BA2.NE.0.) TEXI(4,J1) =TEXI(2,J1) +TOVT
0251      IF (BA2.NE.0..AND.TMIT.NE.0..AND.TEXI(4,J1).LT.TMIT)TEXI(4,J1)=TMIT
0252      QK(J1) = 0.
0253      QR(J1) = 0.
0254      DO 47 NJ=1,NFLX
0255      QK(J1) =QK(J1) + EXI(NJ,J1)*COK(NJ)
0256      QR(J1) =QR(J1) + EXI(NJ,J1)*COR(NJ)
0257      JP =J1+1
0258      QLYS(J1) =EXI(10,J1)
0259      47 CONTINUE
0260      48 CONTINUE

C
C   CALCULATION OF TOTAL HEATING OR COOLING EFFECT
0261      DO 232 J=1,NDT
0262      232 QMAX(J) = QMAS(J)*(CQAK+CQAR)
0263      CQ2 = CQAK +CQAR
0264      IF (CQ2.EQ.0.) GOTO 41
0265      CQK = CQAK/CQ2
0266      CAP = CQAR/CQ2
0267      DO 233 J=1,NDT
0268      233 QMIN(J) = QMIS(J)*(CQIK+CQIR)
0269      CQ2 = CQIK +CQIR
0270      IF (CQ2.EQ.0.) GOTO 41
0271      CIP =CQIR/CQ2
0272      CIK =CQIK/CQ2
0273      DO 181 J2 =1,4
0274      TEXI(J2,NDT+1) = TEXI(J2,1)
0275      181 CONTINUE

C
C   PRINTOUT OF TIMESERIES FOR INPUT TEMPERATURES, FLUXES AND HEATING-
C   AND COOLING EFFECTS
0276      CALL SFLUX(EXI,NFLX,NDT,QMAS,QMIS,IY,IM,IO)
0277      WRITE (6,782) CQAK,CQIK,(COK(N7),N7=1,NFLX),COK(10)
0278      WRITE (6,783) CQAR,CQIR,(COR(N8),N8=1,NFLX),COR(10)
0279      782 FORMAT (1H ,30X,4HKNV ,F9.4,(8F10.4))
0280      783 FORMAT (1H ,30X,4HRADI ,F9.4,(8F10.4))
0281      RETURN
0282      300 STOP
0283      END

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SFLUX

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0001      SUBROUTINE SFLUX(EXT,NFLU,NDT,OMAS,OMIS,IY,IM,ID)
C      PRINTOUT OF TIMESERIES FOR INPUT TEMPERATURES, FLUXES AND HEATING-
C      AND COOLING EFFECTS
0002      COMMON Z(18), QO(50), QK(50), QR(50), QMAX(50), QMI(50),
0003      ITEXI(4,50), IFL(12,50), VENT(12,50)
0004      RE INFL
0005      DIMENSION EXI(10,50), OMAS(50), OMIS(50), NR(10)
0006      DIMENSION SEXI(10)
0007      DIMENSION FLU(10)
0008      DATA FLU / 10*4HFLUX /
0009      DO 10 N=1,10
0010      SEXI(N) = 0.
0011      WRITE (6,111) Z
0012      111 FORMAT (1H1,18A4)
0013      MI=10
0014      WRITE (6,19) ( FLU(M),M,M=1,NFLU),FLU(10),MI
0015      DO 11 I=1,NDT
0016      IT = I
0017      IF (NDT.EQ.24) GO TO 12
0018      TDS = NDT/24
0019      TI = I
0020      IT = TI/TDS
0021      TD = (FLDAT(IT))*TDS
0022      IF (TD.EQ.TI) GO TO 12
0023      WRITE (6,15) ITEXI(1,I), ITEXI(3,I), ITEXI(4,I), OMAS(I), OMIS(I),
0024      I(EXT(N,I),N=1,NFLU), EXI(10,I)
0025      GO TO 14
0026      12 WRITE (6,16) IT, ITEXI(1,I), ITEXI(3,I), ITEXI(4,I), OMAS(I), OMIS(I),
0027      I(EXT(N,I),N=1,NFLU), EXI(10,I)
0028      14 CONTINUE
0029      DO 17 N=1,NFLU
0030      SEXI(N) = SEXI(N) + EXI(N,I)
0031      SEXI(10) = SEXI(10) + EXI(10,I)
0032      17 CONTINUE
0033      DO 20 N=1,10
0034      SEXI(N) = SEXI(N) *24./FLOAT(NDT)
0035      WRITE (6,18) (SEXI(N),N=1,NFLU), SEXI(10)
0036      18 FORMAT (1H,13,(12F10.1))
0037      19 FORMAT (1H,13,(12F10.1))
0038      19 FORMAT (1H,13SUM,50X,10F10.1)
0039      19 FORMAT (1H,13SPECIFIED TEMPERATURES AND FLUXES:/'/' H AIRT 1'
0040      1, AIRT 3 (AIRT 4) OMAX QMIN ',(6(4X,A4,12)) )
0041      RETURN
0042      END

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0001      SUBROUTINE DISKL(NMD,NDG)
C      READS WEATHER DATA FROM CONCENTRATED 'TEST REFERENCE YEAR' ON DISK
0002      COMMON /KDRCL/ AS(50), H(50), RNT(24), RDT(24), TT(24), FF(24), SO, SN
0003      1, RTOT(24), TD(24), NN(24)
0004      DIMENSION IA(30)
0005      DATA ICA, ICB, ICC, ICD, ICE, ICF, ICG, ICH, ICI, ICJ, ICK / 1H1,1H2,1H3,
0006      1H4,1H5,1H6,1H7,1H8,1H9,1H0,1H /
0007      C FOR DECODING CLOUD COVER DATA
0008      NQ = NV(24)
0009      DO 1 J=1,6
0010      READ (1,5) IA
0011      5 FORMAT (13,11,4(14,413,A1,12))
0012      DO 2 K=1,4
0013      KK = K*7 -4
0014      JK = J*4 +K -4
0015      TT(JK) = FLOAT(IA(KK))/10.
0016      C DEWPOINT TEMPERATURE, IN DATASET INCREASED WITH 50.
0017      TD(JK) = FLOAT(IA(KK+1))/10. -50.
0018      RTOT(JK) = IA(KK+2)
0019      RDT(JK) = IA(KK+3)
0020      RNT(JK) = IA(KK+4)
0021      IAA = IA(KK+5)
0022      FF(JK) = IA(KK+6)
0023      C MISSING CLOUD COVER IS SUBSTITUTED BY PRECEDING VALUE
0024      IF (IAA.EQ.ICJ) NQ = 0
0025      IF (IAA.EQ.ICA) NQ = 1
0026      IF (IAA.EQ.ICB) NQ = 2
0027      IF (IAA.EQ.ICC) NQ = 3
0028      IF (IAA.EQ.ICD) NQ = 4
0029      IF (IAA.EQ.ICE) NQ = 5
0030      IF (IAA.EQ.ICF) NQ = 6
0031      IF (IAA.EQ.ICG) NQ = 7
0032      IF (IAA.EQ.ICH) NQ = 8
0033      C N = 9 SUBSTITUTED WITH N = 8
0034      IF (IAA.EQ.ICI) NQ = 8
0035      6 NN(JK) = NQ
0036      2 CONTINUE
0037      1 CONTINUE
0038      NMD = IA(1)/50
0039      NDG = IA(1) -NMD*50
0040      NMD = NMD +1
0041      RETURN
0042      END

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SUNR

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0001      SUBROUTINE SUNR(NMD,NDG,NDN,NBA2,BA2,BAS)
0002      C CALCULATION OF SOLAR ANGLES PER HALF-HOUR, AND SUNRISE AND SUNSET
0003      COMMON /KORS/ AS(50),H(50),RNT(24),RDT(24),TT(24),FF(24),SO,SN
0004      1,RTOT(24),TD(24),NN(24)
0005      DIMENSION DM(12),E(12),QQR(12),RRQ(12)
0006      DATA DM /0.,31.,59.,90.,120.,151.,181.,212.,243.,273.,304.,334./
0007      DATA E /09.,12.,14.,16.,18.,21.,23.,23.,18.,15.,11 /
0008      DATA QQR /2.,39.,3.,065,0.0,3*-.12,-.06,2*.39 /
0009      DATA RRQ /2*.078,3*.121,.127,3*.142,.142,2*.078 /
0010      C FOR 56 DG NORTHERN LATITUDE (SINBR, COSBR)
0011      C SINBR=SIN(LOCAL LATITUDE); TO BE INSERTED IN THE FOLLOWING STATEMENT
0012      DATA SINBR /0.829 /
0013      PJ=0.01745
0014      PI=3.14159
0015      IF (BA2.EQ.0.) GOTO 180
0016      DO 179 I=1,24
0017      179 NN(I)=NBA2
0018      IF (BAS.EQ.0.) GOTO 180
0019      SINBR=SIN(BAS*PJ)
0020      180 CONTINUE
0021      COSBR=SQRT(1.-SINBR**2)
0022      DN=DM(NMD)*FLOD(NDG)
0023      DA=COS(DN*PI/182.5)
0024      DA=1.+0.0334*DA
0025      NDN=DN
0026      H(1)=0.
0027      C TIME EQUATION, AND LOCAL TIME FOR COPENHAGEN 9.7 MINUTES
0028      IF (DN.GE.21.) GOTO 187
0029      TEQ=-2.6-.44*DN
0030      GO TO 186
0031      187 IF (DN.GE.136.) GOTO 188
0032      TEQ=-5.2-9.*COS((DN-43.)*.0357)
0033      GO TO 186
0034      188 IF (DN.GE.241) GOTO 189
0035      TEQ=-1.4+5.*COS((DN-135.)*.0449)
0036      GO TO 186
0037      189 IF (DN.GE.336) GOTO 190
0038      TEQ=6.3+10.*COS((DN-306.)*.0360)
0039      GO TO 186
0040      190 TEQ=-0.46*(DN-359.)
0041      186 CONTINUE
0042      C LOCAL TIME IS INSERTED IN THE FOLLOWING STATEMENT
0043      TET=(TEQ-9.7)/60.
0044      TEQ=TET*PI/12.
0045      DF=DN*PI/182.5
0046      VA=(0.37-22.96*COS(DF)-0.37*COS(2.*DF)-0.15*COS(3.*DF)
0047      1+4.*COS(SIN(DF)*PJ)
0048      SINVA=SIN(VA)
0049      COSVA=COS(VA)
0050      C SUNRISE AND SUNSET, INCLUDING REFRACTION
0051      TON=(SINBR*SINVA+0.01)/(COSBR*COSVA)
0052      TON=(12./PI)*ARCOS(TON)
0053      SO=TON-TET
0054      SN=24.-TON-TET
0055      C SOLAR HEIGHT AND AZIMUTH, PER HALF-HOUR, DEGREES
0056      DO 80 I=1,48
0057      TP=PI*FLOD(I)/24.+TEQ
0058      COSTP=COS(TP)
0059      SINUH=SINVA*SINBR-COSVA*COSBR*COSTP
0060      H2=ARSIN(SINUH)
0061      COSIH=COS(H2)
0062      IF (H2.GT.-0.005) H2=H2+0.000225/(H2+0.023)
0063      SINUH=SIN(H2)
0064      AN=SINBR*COSVA*COSTP+COSBR*SINVA
0065      AN=AN/COSIH
0066      IF ((AN+1.).LT.1.E-5) GOTO 755
0067      AN=ARCOS(AN)
0068      GO TO 786
0069      755 AN=PI
0070      786 AZ=AN-PI
0071      IF (TP.GT.PI) AZ=-AZ
0072      H(I+1)=H2/PJ
0073      AS(I+1)=AZ/PJ
0074      IF (BA2.EQ.0.) GOTO 80
0075      EXT=E(4MD)
0076      CC=NBA2
0077      IF (CC.EQ.1.) CC=0.5
0078      IF (CC.EQ.7.) CC=7.3
0079      IF (CC.GT.8.) CC=8.
0080      Q=-QQR(NMD)*0.1
0081      R=-RRQ(NMD)*0.1
0082      CCF=1.0+Q*CC+R*CC*CC
0083      CQ=(.58+.025*CC*CC-.000288*CC**4)*CC
0084      IF (CQ.GT.8.) CQ=8.
0085      J=(I+1)/2
0086      IF ((I-2*J).EQ.0) GOTO 80
0087      IF (H2.LE.0.) GOTO 81
0088      FL=1.02/(SINUH+.02)
0089      SM=1163.*EXP(-EXT*FL)*DA
0090      HH=0.333*(1370.*DA-SM)*SINUH
0091      RNT(J)=SM*(1.-CQ/8.)
0092      RTOT(J)=(HH+SM*SINUH)*CCF
0093      RDT(J)=RTOT(J)-RNT(J)*SINUH
0094      GO TO 80
0095      81 RNT(J)=0.
0096      RDT(J)=0.
0097      RTOT(J)=0.
0098      80 CONTINUE
0099      RETURN
0100      END

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0001      SUBROUTINE SOLIN(NDP)
C      SOLAR HEAT LOAD THROUGH ROOF, WALLS AND WINDOWS, WITH SUNSHADING
C      HORM = ALTITUDE OF HORIZON, DG.
C      RIBM = RIB, ADJACENT TO WINDOW, DISTANCE AND PROTRUSION
C      UDHM = CANOPY, DISTANCE AND PROTRUSION
C      FM = WINDOW, GLASS, HEIGHT AND WIDTH
C      BEVM = MOVABLE SUNSHADING, SETTING VALUE AND REDUCTION
C      FORDM = FRACTION OF SOLAR GIVEN CONVECTIVELY, WITHOUT AND WITH SHADING
C      TGK = ROOF AREA*(U-VALUE) VAEK = WALL AREA*(U-VALUE)
0002      COMMON /KORS/ AS(50),H(50),RNT(24),RDT(24),TT(24),FF(24),SD,SN
0003      1,RTOT(24),TD(24),NN(24)
0004      COMMON /INTERP/ SCL(50,2),SOLT(50),TVIN(50),TOD(50),TD1(50)
0005      1,MBA(4,50)
0006      COMMON /SR/HORM(10),VAEK(10),UDHM(2,10),RIBM(2,10),BEVM(3,10),
0007      IFM(2,10),FORDM(2,10),VIN(10),AVT(10),TGK
0008      DIMENSION SNT(50),SDT(50)
0009      PJ = 0.01745
0010      TR = 0.76
0011      RF = 0.66
0012      AT = TGK*0.0085
0013      ISD = 2.*SD + 1.1
0014      ISN = 2.*SN + 1.9
0015      SOLT(1) = SOLT(49)
0016      DO 2 I = 2,49
0017      SNT(I) = 0.
0018      12 SNT(I) = 0.
0019      DO 11 I = 100,ISN
0020      IA = I/2
0021      IB = (I-1)/2
0022      SNT(I) = (RNT(IA) + RNT(IB))/2.
0023      SNT(I) = (RDT(IA) + RDT(IB))/2.
0024      11 CONTINUE
0025      DO 20 I = 2,49
0026      DO 13 J = 1,4
0027      MBA(J,I) = 0
0028      TVIN(I) = 0
0029      SCL(I,1) = 0.
0030      SCL(I,2) = 0.
0031      SOLT(I) = SOLT(I-1)*0.4
0032      IF (I.LT.150.OR.I.GT.200) GOTO 20
0033      SCLV = SNT(I)*SCL(I,1)*H(I)*PJ + SDT(I)
0034      C SOLAR HEAT THROUGH ROOF
0035      SOLT(I) = SOLT(I) + SCLV*AT
0036      COSIH = COS(H(I)*PJ)
0037      DO 10 IP = 1,10
0038      VVK = VAEK(IP)*0.0085
0039      AV = AVT(IP)
0040      IF (AV.LE.0..AND.VVK.LE.0.) GOTO 10
0041      14 X = (AS(I) - VIN(IP))*PJ
0042      ZAN = COSIH*COS(X)
0043      VH = AS(I)*S(ZAN)
0044      VAF = 1
0045      FK = 0.
0046      FV = 0.
0047      F = 0.45 + 0.437*ZAN + 0.313*ZAN*ZAN
0048      IF (ZAN.LT.-.2) F = 0.45
0049      C CORRECTION FOR CLOUD COVER
0050      J = I/2
0051      BN = NN(J)
0052      F = (F-.5)*(8.-BN)/8. +.5
0053      DIFD = SDT(I)*F
0054      IF (ZAN) 16,16,201
0055      201 VI = VH/PJ
0056      FV = ZAN
0057      FK = TR*(1.-0.04*(VI/100.)-2.933*(VI/100.)**6+2.13*(VI/100.)**12)
0058      16 IF (H(I).LT.HORM(IP)) GOTO 17
0059      SCLD = SNT(I)*FV
0060      DIFR = SCLV*0.125
0061      GO TO 18
0062      17 SCLD = 0
0063      R = SDT(I)*0.125
0064      C SOLAR HEAT THROUGH WALLS
0065      18 SOLT(I) = SOLT(I) + (SCLD + DIFD + DIFR)*VVK
0066      C FIXED, OUTSIDE SUNSHADINGS, CANOPIES AND VERTICAL 1BS
0067      FMH = FM(1,IP)
0068      FMB = FM(2,IP)
0069      ASU = 1.
0070      ASR = 1.
0071      ADJ = 1.
0072      UDHF = UDHM(2,IP)
0073      RIBF = RIBM(2,IP)
0074      IF (UDHF.LE.0.) GOTO 71
0075      COTA = COS(X)*COSIH/ SIN(H(I)*PJ)
0076      UDHA = UDHM(1,IP)
0077      ASU = (FMH - UDHF/COTA + UDHA)/FMH
0078      IF (ASU.GT.1.) ASU = 1.
0079      IF (ASU.LT.0.) ASU = 0.
0080      TG = UDHF/(UDHA + FMH/2.)
0081      ADJ = 1./SQRT(1.+TG*TG)
0082      71 IF (RIBF.LE.0.) GOTO 72
0083      R13A = RIBM(1,IP)
0084      ASS = RIBF*TAN(X)
0085      ASR = (FMB + R13A - ABS(ASS))/FMB
0086      IF (ASR.GT.1.) ASR = 1.
0087      IF (ASR.LT.0.) ASR = 0.
0088      72 ASU = ASU*ASR
0089      SCLD = SCLD*ASU
0090      DIFD = DIFD*ADJ
0091      C SOLAR HEAT THROUGH WINDOWS
0092      IF (AV.LE.0.) GOTO 10
0093      SOLG = SCLD*FK + (DIFD + DIFR)*R
0094      C MOVABLE SUNSHADING
0095      IF (SOLG.GT.BEVM(3,IP)) NAF = 2
0096      FORD = FORDM(NAF,IP)
0097      SOLK = SOLG*BEVM(NAF,IP)*AV
0098      SCL(1,1) = SCL(1,1) + SOLK*FORD
0099      SCL(1,2) = SCL(1,2) + SOLK*(1.-FORD)
0100      IF (NAF.EQ.2.AND.IP.LE.4) MBA(IP,I) = 1
0101      IF (VOP.NE.IP) GOTO 10
0102      C INSIDE SURFACE OF WINDOW, OVERTEMPERATURE
0103      TVIN(I) = SOLG*BEVM(NAF,IP)*0.008
0104      10 CONTINUE
0105      20 CONTINUE
0106      RETURN
0107      END

```

FORTRAN IV G LEVEL 21

ADM2

DATE = 76133

```

0001      SUBROUTINE ADM2(IM,NDP,NAT1,NAT,THDD,THD1)
C      ADMINISTRATION OF OUTPUT TABLES
C      NDP=-1 GIVES TABLES WITH ROOM AIR TEMPERATURES
C      0 GIVES FURTHERMORE OPERATIVE TEMPERATURE (AIR - SURFACE MEAN)
C      1 (OR 2,3,4) GIVES FURTHERMORE CL. TEMP TOWARDS WINDOW 1 (2,3,4)
0002      COMMON /AD1/ IT(6,30,13),THA(50),THO(50),THR(50),SUM(11,13)
0003      COMMON /INTERP/ SOL(50,2),SOLTI(50),TVIN(50),TOD(50),TODI(50)
0004      1,M3A(4,50)
0005      THDD =-999999.
0006      THD1 =-999999.
0007      DO 10 I=2,49
0008      IF (NDP) 11,12,13
0009      11 J =1
C      ROOM A.I. TEMPERATURE
0010      TJ =THR(1)
0011      GO TO 16
0012      12 J=3
C      OPERATIVE TEMPERATURE TOWARDS WALLS
0013      TJ =TOD(1)
0014      IF (TJ.GT.THDD) THDD =TJ
0015      16 IT =TJ -9.95
0016      14 IF (IT.LT.1) IT=1
0017      IF (IT.GT.30) IT=30
0018      ITAE(J,IT,IM) = ITAE(J,IT,IM) +1
0019      IF (GLIM(J,1,IM).GT.TJ) GLIM(J,1,IM) =TJ
0020      IF (GLIM(J,2,IM).LT.TJ) GLIM(J,2,IM) =TJ
0021      J=J +1
0022      IF (I.LT.NAT1.OR.1.GT.NAT) GOTO 20
0023      ITAE(J,IT,IM) =ITAE(J,IT,IM) +1
0024      IF (GLIM(J,1,IM).GT.TJ) GLIM(J,1,IM) =TJ
0025      IF (GLIM(J,2,IM).LT.TJ) GLIM(J,2,IM) =TJ
0026      20 IF (J-4) 10,11,12
0027      13 J=5
C      OPERATIVE TEMPERATURE TOWARDS WINDOW
0028      TI =TODI(1)
0029      IF (TI.GT.THDD) THD1 =TI
0030      IT =TI -9.95
0031      17 IF (IT.LT.1) IT=1
0032      IF (IT.GT.30) IT=30
0033      ITAE(J,IT,IM) =ITAE(J,IT,IM) +1
0034      IF (GLIM(J,1,IM).GT.TI) GLIM(J,1,IM) =TI
0035      IF (GLIM(J,2,IM).LT.TI) GLIM(J,2,IM) =TI
C      DIFFERENTIAL OPERATIVE TEMPERATURE WINDOW - WALLS.
0036      TI =TI -(THR(1) +THO(1))/2.
0037      IT =TI +10.
0038      J =J +1
0039      IF (J.EQ.6) GOTO 17
0040      GO TO 12
0041      10 CONTINUE
0042      RETURN
0043      END

```

FORTRAN IV G LEVEL 21

INPOL

DATE = 76133

```

0001      SUBROUTINE INPOL(NULT,TOVT,TMIT)
C      INTERPOLATES OUTDOOR AIR TEMP. AND VENTILATION TEMP., HALF-HOUR VALUE
0002      COMMON T(18),OO(50),OK(50),OR(50),QMAX(50),OMIN(50),
0003      ITEXI(4,50),INFL(12,50),VENT(12,50)
0004      COMMON /KORS/ AS(50),H(50),RNT(24),RDT(24),TT(24),FF(24),SD,SN
0005      1,RTOT(24),TD(24),NN(24)
0006      REAL NULT
0007      DO 111 I=2,24
0008      13 =I*2
0009      12 =13 -1
0010      TEXI(2,13) =TT(1)
0011      TEXI(2,12) =(TT(1) +TT(I-1))/2.
0012      TEXI(2,1) =(TT(1) +NULT)/2.
0013      TEXI(2,2) =TT(1)
0014      NULT =TT(24)
0015      IF (TMIT.EQ.0.) GOTO 114
0016      DO 113 I=1,48
0017      TEX =TEXI(2,I) +IOVT
0018      IF (TEX.LT.TMIT) TEX =TMIT
0019      TEXI(4,I) =TEX
0020      113 CONTINUE
0021      114 CONTINUE
0022      RETURN
0023      END

```


FORTRAN IV G LEVEL 21

FRAKT

DATE = 75133

```

0001      SUBROUTINE FRAKT(J,FRAK)
0002      C CALCULATION OF FRACTILES, 0/0, 50 0/0 AND 90 0/0
      COMMON /AD1/ ITAEL(5,30), THA(50), THD(50), THF(50), SUM(11,13)
0003      1, GLIM(6,2,13)
      DIMENSION IT(30), FRAK(1,13)
0004      REAL IT
0005      G6 = 0.
0006      IF (J.EQ.6) G6 = -20.
0007      DO 11 M=1,13
0008      IT(1) = ITAEL(J,1,M)
0009      DO 10 I=2,30
0010      10 IT(I) = IT(I-1) + FLDAT(ITAEL(J,I,M))
0011      DO 12 I=1,3
0012      AN = IT(30) + (I*.4 - 0.3)
0013      DO 13 I=1,30
0014      13 IF (AN.GT.IT(I)) IC = I + 1
      C STRAIGHT OR CURVED INTERPOLATION, DEPENDANT ON THE CURVATURE OF
      C THE ADJACENT SEGMENTS.
0015      IF (IC.LT.3.OR.IC.GT.28) GOTO 101
0016      A = IT(I-2)
0017      D = IT(I-1)
0018      94 C = IT(IC)
0019      B = IT(IC-1)
0020      GC = FLDAT(IC) + 11. + G6
0021      GB = GC - 1.
0022      IF (GLIM(J,1,M).GT.GB) GB = GLIM(J,1,M)
0023      IF (GLIM(J,2,M).LT.GC) GC = GLIM(J,2,M)
0024      DO 90 I=1,10
0025      AM = (FLDAT(I) - 0.5)*0.1
0026      XA = B + AM*(B - A)
0027      XD = C - (1.-AM)*(D - C)
0028      XR = 0.5*AM*(1.-AM)*(B + C - A - D)
0029      XM = B + AM*(C - B)
0030      XX = XM + XR
0031      XAD = 2*B - A - C
0032      XDD = 2*C - D - B
0033      IF (XAD.EQ.0..OR.XD.EQ.0..OR.XR.EQ.0.) GOTO 51
0034      XAD = XAD/XDD
0035      IF (XAD.LT.0.) GOTO 51
0036      IF (XR.GT.0.) GOTO 53
0037      IF (XX.GE.XA.AND.XX.GE.XD) GOTO 52
0038      XX = XA
0039      IF (XD.GT.XA) XX = XD
0040      GO TO 52
0041      53 IF (XX.LE.XA.AND.XX.LE.XD) GOTO 52
0042      XX = XA
0043      IF (XD.LT.XA) XX = XD
0044      GO TO 52
0045      51 XX = XM
0046      52 IF (XX.GT.AN) GOTO 91
0047      90 CONTINUE
0048      91 ANN = FLDAT(I-1)*(GC - GB)*0.1 + GB
0049      GO TO 92
0050      101 IF (IC.NE.2.AND.IC.NE.29) GOTO 102
0051      A = IT(IC-1)
0052      D = IT(IC)
0053      GOTO 94
0054      102 ANN = 999999.
0055      92 FRAK(I1,M) = ANN
0056      12 CONTINUE
0057      11 CONTINUE
0058      RETURN
0059      END

```

FORTRAN IV G LEVEL 21

TAPL

DATE = 78125

```

0001      SUBROUTINE TAPL(NMD,NDG)
0002      C READS WEATHER DATA FROM 'TEST REFERENCE YEAR' ON TAPE
      COMMON /KORS/ AS(50), H(50), RNT(24), RDT(24), TT(24), FF(24), SO, SN
0003      1, RTOT(24), TD(24), NN(24)
      DATA ICA, ICB, ICC, ICD, ICE, ICF, ICG, ICH, ICI, ICJ, ICK / 1H1, 1H2, 1H3,
      11H4, 1H5, 1H6, 1H7, 1H8, 1H9, 1H0, 1H /
      C FOR DECODING CLOUD COVER DATA
0004      NQ = NN(24)
0005      DO 1 J=1, 24
0006      READ (1,5) I1, I2, I3, I4, I5, IAA, I6, NMD, NDG
0007      5 FORMAT (2I4, 15X, 3I3, 3X, A1, 2X, I2, 34X, 2I2, 2X)
0008      TT(J) = FLOAT(I1)/10.
0009      TD(J) = FLOAT(I2)/10.
0010      RTOT(J) = FLOAT(I3)
0011      RDT(J) = FLOAT(I4)
0012      RNT(J) = FLOAT(I5)
0013      FF(J) = FLOAT(I6)
      C MISSING CLOUD COVER IS SUBSTITUTED BY PRECEDING VALUE
0014      IF (IAA.EQ.ICJ) NQ = 0
0015      IF (IAA.EQ.ICA) NQ = 1
0016      IF (IAA.EQ.ICB) NQ = 2
0017      IF (IAA.EQ.ICC) NQ = 3
0018      IF (IAA.EQ.ICD) NQ = 4
0019      IF (IAA.EQ.ICE) NQ = 5
0020      IF (IAA.EQ.ICF) NQ = 6
0021      IF (IAA.EQ.ICG) NQ = 7
0022      IF (IAA.EQ.ICH) NQ = 8
      C
      C N = 9 SUBSTITUTED WITH N = 8
      IF (IAA.EQ.ICI) NQ = 8
0023      NN(J) = NQ
0024      1 CONTINUE
0025      RETURN
0026      END
0027

```

BA4 PROGRAM. Example of input cards and output

Input Cards:

KONTROLBEREGNING BAZHL, MAJ 1974. REFERENCEAR

TU	E1.
----	-----

TO 1240.

TA 250.

TK	0.
----	----

18 1740.

title card

```

} room data

```

blank card
excitations

VINDUE	1	3.0	-45.
--------	---	-----	------

INCIDENT 7.

BEV. AFSK	1	150.	0.6
-----------	---	------	-----

FOR	1	0.5	0.5
-----	---	-----	-----

AIRTEL 1

AIRTEMP	4	0.	-30.
---------	---	----	------

FLUX 1

8.3

FLUX	1 0.5	0.5
------	-------	-----

ELLYS	100.
-------	------

FLUX 10

0. 0.

2. 2

8.25	150.
------	------

17.	150.
-----	------

17.25	0
-------	---

24.

FLUX	10 0.5	0.5
------	--------	-----

VENT II

0. 11 30.

5.101 30.

6.20	50.
------	-----

18.10	€0.
-------	-----

18.19	30.
-------	-----

24. 11 30.

QMAX 11

0.	3000.
----	-------

24. 11 3000.

OPER	1
------	---

UDSKRIV	6.03	12.01
---------	------	-------

LASTFLUX

blank card

Printout from run:

Year Month Day of job run.
1976 - 5 - 13

KONTROLBEREGNING BA/HL, MAJ 1974. REFERENCEAAR Title

LAB. FOR VARMEISOLERING, DTH, PROGRAM BA4(MAJ76)

TU = 21.00 TK = 0.0 TO = 240.00 TA = 690.00 } Room data
S = 1740.00 DT = 0.50

VINDUE	1	3.000	-45.000	Window , area m ² and direction SE
HORISONT	0	7.000	0.0	Horizon 7°
BEV.AFSK	1	150.000	0.600	Movable sunshading
FORDEL	1	0.500	0.500	Convective part without and with sunshading
AIRTEMP	1	0.0	0.0	Desired airtemperature , see next page
AIRTEMP	4	0.0	-30.000	Ventilation air (primary air) outside , no tempera- ture increase
FLUX	1	0.0	0.0	Time serie , see next page (persons)
FLUX	1	0.500	0.500	Convective and radiative part
ELLYS	0	100.000	0.0	Electric light if sunradiation less than 100W through the window
FLUX	10	0.0	0.0	" " , time serie
FLUX	10	0.500	0.500	Convective and radiative part
VENT	0	0.0	0.0	Ventilation , time serie
0.0		30.00000		
6.10		30.00000		Reduced ventilation
6.20		60.00000		during the night.
18.10		60.00000		
18.20		30.00000		
24.00		30.00000		
QMAX	0	0.0	0.0	Max heat load , time serie
OPER	1	0.0	0.0	Operative temp. and directional operative temp. desired
UDSKRIV	0	6.030	12.010	Print-out of June, 3rd and December 1st desired
LASTFLUX	0	0.0	0.0	No more excitations

SPECIFIED TEMPERATURES AND FLUXES

H	AIRT 1	AIRT 3	(AIRT 4)	QMAX	QMIN	FLUX 1	FLUX10
1	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
2	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
3	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
4	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
5	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
6	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
7	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
8	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
9	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
10	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
11	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
12	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
13	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
14	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
15	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
16	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
17	21.0	0.0	0.0	3000.0	0.0	120.0	150.0
18	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
19	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
20	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
21	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
22	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
23	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
24	21.0	0.0	0.0	3000.0	0.0	0.0	0.0
SUM			KONV RADI	1.0000 0.0	1.0000 0.0	1080.0 0.5000 0.5000	1350.0 0.5000 0.5000

KONTROL	MD	DG	RLT	M	KL	RLT	MAX	MAJ	1974.	REFERENCE	Q	KOLE	Q	VARM	Q	PRIM	1976	Q	SOL	5	-	13	UVQ	E-L	B-A1
1	1	1	21.0	21.0	5.30	21.0	21.0	OP-T	20.8	17.3	0.	0.	0.	26149.	0.	0.	92.	0.	0.	0.	0.	0.	0.	18	0
1	1	2	21.0	21.0	0.30	21.0	21.0	OP-T	20.5	17.5	0.	0.	0.	26189.	0.	0.	309.	0.	0.	0.	0.	0.	0.	18	0
1	1	3	21.0	21.0	2.30	21.0	21.0	OP-T	20.5	17.7	0.	0.	0.	26209.	0.	0.	56.	0.	0.	0.	0.	0.	0.	18	0
1	1	4	21.0	21.0	2.30	21.0	21.0	OP-T	20.5	17.9	0.	0.	0.	26080.	0.	0.	581.	0.	0.	0.	0.	0.	0.	15	0
1	1	5	21.0	21.0	1.30	21.0	21.0	OP-T	20.4	17.2	0.	0.	0.	27648.	0.	0.	184.	0.	0.	0.	0.	0.	0.	18	0
1	1	6	21.0	21.0	6.30	21.0	21.0	OP-T	20.4	17.7	0.	0.	0.	27365.	0.	0.	676.	0.	0.	0.	0.	0.	0.	12	0
1	1	7	21.0	21.0	0.30	21.0	21.0	OP-T	20.4	17.3	0.	0.	0.	27821.	0.	0.	218.	0.	0.	0.	0.	0.	0.	18	0
1	1	8	21.0	21.0	4.00	21.0	21.0	OP-T	20.5	17.1	0.	0.	0.	29390.	0.	0.	379.	0.	0.	0.	0.	0.	0.	18	0
1	1	9	21.0	21.0	1.00	21.0	21.0	OP-T	20.4	17.5	0.	0.	0.	26214.	0.	0.	212.	0.	0.	0.	0.	0.	0.	18	0
1	1	10	21.0	21.0	2.00	21.0	21.0	OP-T	20.4	17.3	0.	0.	0.	27214.	0.	0.	137.	0.	0.	0.	0.	0.	0.	18	0
1	1	11	21.0	21.0	4.30	21.0	21.0	OP-T	20.4	16.9	0.	0.	0.	30417.	0.	0.	292.	0.	0.	0.	0.	0.	0.	18	0
1	1	12	21.0	21.0	22.00	21.0	21.0	OP-T	20.6	18.3	0.	0.	0.	29359.	0.	0.	4620.	0.	0.	0.	0.	0.	0.	16	9
1	1	13	21.0	21.0	0.30	21.0	21.0	OP-T	20.5	17.6	0.	0.	0.	26425.	0.	0.	127.	0.	0.	0.	0.	0.	0.	18	9
1	1	14	21.0	21.0	0.30	21.0	21.0	OP-T	20.7	18.6	0.	0.	0.	24983.	0.	0.	3567.	0.	0.	0.	0.	0.	0.	14	9
1	1	15	21.0	21.0	3.00	21.0	21.0	OP-T	20.5	17.9	0.	0.	0.	25766.	0.	0.	872.	0.	0.	0.	0.	0.	0.	8	2
1	1	16	21.0	21.0	0.30	21.0	21.0	OP-T	20.6	18.6	0.	0.	0.	25825.	0.	0.	3833.	0.	0.	0.	0.	0.	0.	8	8
1	1	17	21.0	21.0	6.00	21.0	21.0	OP-T	20.4	17.5	0.	0.	0.	29123.	0.	0.	955.	0.	0.	0.	0.	0.	0.	8	9
1	1	18	21.0	21.0	3.00	21.0	21.0	OP-T	20.6	18.3	0.	0.	0.	29403.	0.	0.	3985.	0.	0.	0.	0.	0.	0.	8	9
1	1	19	21.0	21.0	0.30	21.0	21.0	OP-T	20.6	18.2	0.	0.	0.	29529.	0.	0.	3771.	0.	0.	0.	0.	0.	0.	8	8
1	1	20	21.0	21.0	1.30	21.0	21.0	OP-T	20.5	18.0	0.	0.	0.	29216.	0.	0.	3247.	0.	0.	0.	0.	0.	0.	8	8
1	1	21	21.0	21.0	0.30	21.0	21.0	OP-T	20.5	18.2	0.	0.	0.	28435.	0.	0.	3225.	0.	0.	0.	0.	0.	0.	8	8
1	1	22	21.0	21.0	6.30	21.0	21.0	OP-T	20.4	17.4	0.	0.	0.	30514.	0.	0.	2038.	0.	0.	0.	0.	0.	0.	15	7
1	1	23	21.0	21.0	23.00	21.0	21.0	OP-T	20.4	17.9	0.	0.	0.	30908.	0.	0.	995.	0.	0.	0.	0.	0.	0.	8	2
1	1	24	21.0	21.0	7.00	21.0	21.0	OP-T	20.4	17.1	0.	0.	0.	33739.	0.	0.	2751.	0.	0.	0.	0.	0.	0.	8	9
1	1	25	21.0	21.0	9.30	21.0	21.0	OP-T	20.4	17.4	0.	0.	0.	35180.	0.	0.	3943.	0.	0.	0.	0.	0.	0.	8	9
1	1	26	21.0	21.0	2.00	21.0	21.0	OP-T	20.4	17.8	0.	0.	0.	36168.	0.	0.	4463.	0.	0.	0.	0.	0.	0.	6	6
1	1	27	21.0	21.0	2.00	21.0	21.0	OP-T	20.4	17.7	0.	0.	0.	34906.	0.	0.	4228.	0.	0.	0.	0.	0.	0.	6	6
1	1	28	21.0	21.0	1.00	21.0	21.0	OP-T	20.5	18.0	0.	0.	0.	29910.	0.	0.	308.	0.	0.	0.	0.	0.	0.	18	10
1	1	29	21.0	21.0	1.00	21.0	21.0	OP-T	20.8	19.4	0.	0.	0.	25270.	0.	0.	604.	0.	0.	0.	0.	0.	0.	14	0
1	1	30	21.0	21.0	1.30	21.0	21.0	OP-T	20.5	18.5	0.	0.	0.	20738.	0.	0.	2090.	0.	0.	0.	0.	0.	0.	10	0
1	2	31	21.0	21.0	0.30	21.0	21.0	OP-T	20.6	18.2	0.	0.	0.	24116.	0.	0.	1235.	0.	0.	0.	0.	0.	0.	10	6
2	2	1	21.0	21.0	23.00	21.0	21.0	OP-T	20.8	19.3	0.	0.	0.	21891.	0.	0.	620.	0.	0.	0.	0.	0.	0.	12	0
2	2	2	21.0	21.0	22.30	21.0	21.0	OP-T	20.6	18.7	0.	0.	0.	20563.	0.	0.	3801.	0.	0.	0.	0.	0.	0.	10	6
2	2	3	21.0	21.0	0.30	21.0	21.0	OP-T	20.7	18.3	0.	0.	0.	22295.	0.	0.	470.	0.	0.	0.	0.	0.	0.	18	9
2	2	4	21.0	21.0	4.00	21.0	21.0	OP-T	20.6	18.7	0.	0.	0.	23205.	0.	0.	2821.	0.	0.	0.	0.	0.	0.	6	7
2	2	5	21.0	21.0	1.30	21.0	21.0	OP-T	20.6	17.9	0.	0.	0.	28794.	0.	0.	2906.	0.	0.	0.	0.	0.	0.	7	10
2	2	6	21.0	21.0	2.30	21.0	21.0	OP-T	20.4	17.3	0.	0.	0.	30628.	0.	0.	4395.	0.	0.	0.	0.	0.	0.	6	10
2	2	7	21.0	21.0	1.30	21.0	21.0	OP-T	20.7	18.9	0.	0.	0.	30797.	0.	0.	489.	0.	0.	0.	0.	0.	0.	16	0
2	2	8	21.0	21.0	4.00	21.0	21.0	OP-T	20.8	18.9	0.	0.	0.	23369.	0.	0.	4164.	0.	0.	0.	0.	0.	0.	5	11
2	2	9	21.0	21.0	3.00	21.0	21.0	OP-T	20.5	18.2	0.	0.	0.	23181.	0.	0.	4477.	0.	0.	0.	0.	0.	0.	11	11
2	2	10	21.0	21.0	2.00	21.0	21.0	OP-T	20.8	19.1	0.	0.	0.	25884.	0.	0.	627.	0.	0.	0.	0.	0.	0.	13	0
2	2	11	21.0	21.0	2.00	21.0	21.0	OP-T	20.8	19.0	0.	0.	0.	24304.	0.	0.	4706.	0.	0.	0.	0.	0.	0.	15	11
2	2	12	21.0	21.0	6.30	21.0	21.0	OP-T	20.4	17.0	0.	0.	0.	34977.	0.	0.	1826.	0.	0.	0.	0.	0.	0.	8	4
2	2	13	21.0	21.0	2.30	21.0	21.0	OP-T	20.4	17.4	0.	0.	0.	35799.	0.	0.	3632.	0.	0.	0.	0.	0.	0.	6	7
2	2	14	21.0	21.0	1.00	21.0	21.0	OP-T	20.3	16.8	0.	0.	0.	30537.	0.	0.	1296.	0.	0.	0.	0.	0.	0.	6	0
2	2	15	21.0	21.0	7.00	21.0	21.0	OP-T	20.4	17.2	0.	0.	0.	33204.	0.	0.	980.	0.	0.	0.	0.	0.	0.	9	0
2	2	16	21.0	21.0	15.30	21.0	21.0	OP-T	20.4	17.2	0.	0.	0.	32814.	0.	0.	1830.	0.	0.	0.	0.	0.	0.	6	0
2	2	17	21.0	21.0	6.30	21.0	21.0	OP-T	20.3	16.7	0.	0.	0.	33842.	0.	0.	1095.	0.	0.	0.	0.	0.	0.	6	3
2	2	18	21.0	21.0	6.30	21.0	21.0	OP-T	20.3	16.8	0.	0.	0.	36354.	0.	0.	2416.	0.	0.	0.	0.	0.	0.	6	0

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MONTH 6 DAY 3

KL	RL-T	OP-T	OPTI	UDLI	QREG	QPRIM	QTOF	SOLIND	UVQ	E-L	B-A1
1	21.5	21.9	20.3	14.5	0.0	0.0	0.0	0.0	0	0	0
2	21.4	21.8	20.2	14.4	0.0	0.0	0.0	0.0	0	0	0
3	21.3	21.7	20.1	14.3	0.0	0.0	0.0	0.0	0	0	0
4	21.2	21.6	20.0	14.2	0.0	0.0	0.0	0.0	0	0	0
5	21.0	21.5	19.8	13.9	0.0	0.0	0.0	0.0	0	0	0
6	21.0	21.4	19.7	13.6	23.8	0.0	23.8	0.0	0	0	0
7	21.0	21.3	19.7	13.5	44.1	0.0	44.1	0.0	0	0	0
8	21.0	21.3	19.7	13.5	63.5	0.0	63.5	0.0	0	0	0
9	21.0	21.3	19.7	13.5	61.8	0.0	61.8	0.0	0	0	0
10	21.0	21.3	19.8	13.7	58.1	0.0	58.1	0.0	0	0	0
11	21.0	21.3	20.0	14.5	35.5	0.0	35.5	0.0	0	0	0
12	21.0	21.3	20.1	15.4	11.5	0.0	11.5	0.0	0	0	0
13	21.0	21.3	20.3	15.8	113.0	0.0	113.0	0.0	0	0	0
14	21.0	21.3	20.5	16.2	36.3	0.0	36.3	0.0	0	0	0
15	21.3	21.5	21.0	16.8	0.0	0.0	0.0	0.0	0	0	0
16	22.1	22.0	22.0	17.4	0.0	0.0	0.0	0.0	0	0	1
17	23.0	22.7	23.1	18.4	0.0	0.0	0.0	0.0	0	0	1
18	23.7	23.2	23.9	19.5	0.0	0.0	0.0	0.0	0	0	1
19	24.0	23.5	24.3	20.1	0.0	0.0	0.0	0.0	0	0	1
20	24.3	23.8	24.6	20.7	0.0	0.0	0.0	0.0	0	0	1
21	24.5	24.0	24.9	21.3	0.0	0.0	0.0	0.0	0	0	1
22	24.8	24.3	25.1	21.7	0.0	0.0	0.0	0.0	0	0	1
23	24.9	24.4	25.2	22.0	0.0	0.0	0.0	0.0	0	0	1
24	24.9	24.4	25.2	22.4	0.0	0.0	0.0	0.0	0	0	1
1	25.0	24.6	25.2	23.4	0.0	0.0	0.0	0.0	0	0	1
2	25.1	24.8	25.6	24.0	0.0	0.0	0.0	0.0	0	0	1
3	25.2	25.1	26.0	24.6	0.0	0.0	0.0	0.0	0	0	1
4	25.2	25.2	26.0	25.6	0.0	0.0	0.0	0.0	0	0	1
5	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
6	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
7	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
8	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
9	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
10	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
11	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
12	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
13	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
14	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
15	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
16	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
17	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
18	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
19	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
20	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
21	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
22	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
23	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1
24	25.2	25.2	26.0	26.6	0.0	0.0	0.0	0.0	0	0	1

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AIRTEMPERATURE, FROM 0.0 TO 24.00

HALF-HOURS IN	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR
21.0- 22	1488	1344	1488	1432	1350	950	907	1085	1350	1479	1440	1488	15801
22.0- 23	0	0	0	8	85	207	265	211	73	7	0	0	856
23.0- 24	0	0	0	0	51	109	150	81	17	2	0	0	410
24.0- 25	0	0	0	0	2	65	75	47	0	0	0	0	189
25.0- 26	0	0	0	0	0	42	57	33	0	0	0	0	132
26.0- 27	0	0	0	0	0	46	34	29	0	0	0	0	109
27.0- 28	0	0	0	0	0	21	0	2	0	0	0	0	23
MEAN, DEGREE CENTIGRADE	21.0	21.0	21.0	21.0	21.2	22.0	22.0	21.7	21.1	21.0	21.0	21.0	21.3
QQ- KWH	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
QQ+ KWH	880.2	805.1	738.8	513.8	271.6	74.2	68.9	89.7	185.4	433.6	637.2	917.5	5615.9
QPRIM KWH	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
QTOT KWH	880.2	805.1	738.8	513.8	271.6	74.2	68.9	89.7	185.4	433.6	637.2	917.5	5615.9
QSQL KWH	54.0	73.0	122.1	152.1	153.6	162.7	154.6	136.9	113.8	74.8	43.4	42.6	1283.5
QELYS KWH	28.9	15.7	9.0	2.1	1.5	0.4	0.8	1.7	5.9	16.5	25.6	29.7	138.0
UVQ, HALFHOURS	0	0	0	0	0	0	0	0	0	0	0	0	0
QTOT OCTOBER - APRIL INCL.			4926.1										

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KONTROLBEREGNING BA/HL, MAJ 1974. REFERENCEAAR

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AIRTEMPERATURE, FROM 8.30 TO 17.00

HALF-HOURS IN	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR
21.0- 22	558	504	558	532	441	251	209	306	451	549	540	558	5457
22.0- 23	0	0	0	8	66	128	139	132	72	7	0	0	552
23.0- 24	0	0	0	0	49	58	89	36	17	2	0	0	251
24.0- 25	0	0	0	0	2	25	31	31	0	0	0	0	108
25.0- 26	0	0	0	0	0	21	39	24	0	0	0	0	84
26.0- 27	0	0	0	0	0	36	32	27	0	0	0	0	95
27.0- 28	0	0	0	0	0	21	0	2	0	0	0	0	23

FRACTILES, TEMPERATURES

10 0/0	21.0	21.0	21.0	21.1	21.1	21.2	21.3	21.2	21.1	21.1	21.0	21.0	21.1
50 0/0	21.0	21.0	21.0	21.5	21.6	22.1	22.4	21.9	21.6	21.5	21.0	21.0	21.6
90 0/0	21.0	21.0	21.0	21.9	22.9	26.1	25.3	24.9	22.1	21.9	21.0	21.0	22.6

KONTROLBEREGNING BA/HL, MAJ 1974. REFERENCEAAR

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OPERATIVE TEMPERATURE TOWARD WINDOW 1, FROM 8.30 TO 17.00

HALF-HOURS IN	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR
13.0- 14	0	0	0	0	0	0	0	0	0	0	0	1	1
14.0- 15	0	2	0	0	0	0	0	0	0	0	0	3	5
15.0- 16	14	9	0	0	0	0	0	0	0	0	0	60	83
16.0- 17	122	164	26	0	0	0	0	0	0	0	29	136	477
17.0- 18	361	198	240	20	6	0	0	0	0	3	138	291	1257
18.0- 19	59	125	175	261	40	0	0	0	0	0	328	58	1191
19.0- 20	2	6	113	206	174	9	0	0	0	145	45	9	1004
20.0- 21	0	0	4	40	176	146	15	18	101	306	0	0	975
21.0- 22	0	0	0	7	154	122	123	154	255	21	0	0	575
22.0- 23	0	0	0	6	61	102	103	160	108	3	0	0	461
23.0- 24	0	0	0	0	43	55	67	108	58	3	0	0	217
24.0- 25	0	0	0	0	4	19	51	31	18	0	0	0	108
25.0- 26	0	0	0	0	0	26	40	34	0	0	0	0	81
26.0- 27	0	0	0	0	0	33	33	15	0	0	0	0	94
27.0- 28	0	0	0	0	0	28	3	28	0	0	0	0	41

FRACTILES, TEMPERATURES

10 0/0	16.7	16.4	17.1	18.1	19.1	20.3	20.3	20.3	19.8	18.6	17.4	15.9	17.1
50 0/0	17.4	17.4	18.1	18.9	20.3	21.9	22.3	21.7	20.7	19.4	18.3	17.3	19.2
90 0/0	18.0	18.5	19.4	19.9	22.9	26.2	25.4	24.9	22.2	20.3	18.9	18.1	22.7

Modifications in the BA4 programmeOctober 1981

The BA4 programme has been modified to enable its use for the "Short Reference Year" research programme. A few other modifications have also been included at the same time.

The new version (October 1981) contains all the facilities from earlier versions (April 78 or November 80). Input data for earlier versions can be used without any change with only a few exception.

This paper gives the modifications only and must be considered as an appendix to "BA4 Users Guide", 2. edition 1979.

The new facilities are:

- week and weekend programme for loads, schedules, light and ventilation rates.
- a new specification of deadband between heating and cooling setpoint, and throttling ranges.
- thermostat setpoints specified as room air temperature alone, or a combination of room air temperature and radiation (surface) temperature
- printout of some daily max loads
- latitude and local time (longitude)
- calculation with multiyear periods, selected shorter periods or "Short Reference Years" and weighting of results to full months or year.

The only limitations regarding earlier input data are:

- cooling to a setpoint other than AIRTemp 1 is now specified with T-Stat instead of QMIN NB
- VENT 1 and VENT (blank) overrides each other

Weekend programmes

The programme can handle three sorts of days:

Weekdays, Saturdays and Sundays.

The following new typecard is used:

(FORMAT: A4, 5X, 12, 2F10.3)

WEEKend NB CK CR

This typecard calls the weekend programme. If this typecard is not present all days are handled as weekdays.

NB Week-day-number of the first day on the weather file (e.g. January 1 in the Test Reference Year). 1 = Monday, 2 = Tuesday, etc. Default value = 7 = Sunday.

CK Time for switch-off of daylight-dependant electric light (FLUX 10) or Saturdays. (Blank is read as 0.0).

CR Item for Sundays. .

If WEEKend is specified a number of parameters (typecards) can be specified with a weekend programme. They are:

AIRTemp	1	(desired room temperature)
FLUX	1	(heat load to the room)
VENT	1	(ventilation)
QMAX	1	(max. heating effect)
QMIN	1	(max. cooling effect)
A-TID	1	(working hours, used for output purposes)

NB = 1 indicates that these are valid for weekdays, Monday through Friday, and they must all, but A-TID, be followed by time series (as previously).

AIRTemp 6, FLUX 6, VENT 6, QMAX 6 and QMIN 6 again followed by timeseries, and A-TID 6, give the Saturday values, and AIRTemp 7 etc. give the Sunday values.

AIRTemp 0 (or blank) will be read as AIRTemp 1. The same applies to typecards with FLUX, VENT, QMAX, QMIN and A-TID, and also INFI (infiltration).

If WEEKend is specified, Saturday and Sunday values for AIRTemp, FLUX, VENT etc. must be given, otherwise the corresponding time-series will be zeroed.

Remarks:

1) AIRTemp 2, 3, 4 or 5, and FLUX 2, 3 etc. cannot be used for giving specific values for Tuesday, Wednesday etc. Only Saturdays and Sundays and weekdays can be specified. Only AIRTemp 1 and FLUX 1 can be changed by a weekend programme.

AIRTemp 5 and FLUX 8 and 9 are not allowed and will cause an error message.

2) VENT 2, 3 etc. can still be used for changing VENT 1 for weekdays through specified part of the year.

3) No weekend programme is included for INFIltration.

4) QMAX 2, 3, 4 and 5 and QMIN 2, 3, 4 and 5 have no meaning and will cause an error message.

5) The previously used specification of a cooling temperature thermostat setpoint, different from the heating setpoint, QMIN NB, where NB was the cooling setpoint, is no longer useable. See the following description of thermostat programme.

If the WEEKend typecard is not specified, AIRTemp 1, FLUX 1 etc. will be used for all days.

Latitude

The typecard LATItude gives the geographical location and the type weather input data:

LATItude NB CK CR

NB Weather data reading subroutine

1 (default value) special concentrated "BA4-format",
Test Reference Year (TRY), Short Reference Year (SRY) or
several years.

2 Full Test Reference Year format (Danish).

(3 Special format, for 15-year-dataset. Not included in the present BA4 programme. Can be used for user designed input formats).

CK latitude. deg North. (Negative value for southern hemisphere). Default value 56 deg N, Copenhagen).

CR Local time, minutes. Locations west of time zone longitude negative sign, east of time zone longitude positive sign. Default value - 9.7 minutes, Copenhagen.

Short Reference Year

This typecard contains specifications often used in connection with runs with Short Reference Years (SRY). It is, however, neither mandatory nor exclusively used with SRY-runs.

SRY NB CK

NB Presentation of monthly or trimonthly output. Default value 1.

1 Monthly sums for the actual number of days computed.

2 Trimonthly sums for the actual number of days computed.

December through February printed as January.

March through May printed as April.

June through August printed as July.

September through November printed as October.

3 As 1, but weighted to a full month (28-31 days).

4 As 2, but weighted to a full season.

CK Number of repetitions of the first day in the dataset - TRY or SRY - in order to remove the initial transients in the resulting temperatures and loads. Default values 0.

Thermostat programme

It is now possible to specify more detailed parameters for the thermostat. Typecard is:

T-Stat NB CK CR

- NB Thermostat setpoint for cooling, deg. C. If 0 or blank or less than AIRTemp 1 (or 6 or 7), the latter is used.
- CK Fraction of thermostat sensitivity from room air temperature. The remaining part (1-CK) is then from mean surface temperature.
- CR Throttling range, deg. C, identical for heating and cooling effect. Default value 0.

Remark:

If CK = 0.5 and CR = 0. the thermostat will try to keep the operative temperature (mean of air temperature and surface temperature) at defined value, AIRTemp 1 (or 6 or 7), or NB if cooling.

Running selected periods

The typecard DATO makes it possible to run specified parts of a weather data set

DATO	NB	CK	CR
------	----	----	----

NB Year for start (e.g. 60 ~ 1960). Default value 11 because the Danish TRY is called year 11.

CK Month.day (~XX.YY) for beginning of calculation.
(Default 1.01)

CR Month.day (~XX.YY) for end of calculation. (Default 12.31)

If the calculation includes more than one year two cards are specified:

DATO	NB	CK	year and month.day for start
------	----	----	------------------------------

DATO	NB	CR	year and month.day for end of the calculation
------	----	----	---

Up to 20 periods, in chronological order, can be specified in one run.

Printout

The typecard UDSK has now one more parameter, NB:

UDSKriv NB CK CR

NB Daily printout

-1 Suppresses daily printout (like CK = -1. or
CR = -1. does).

2 Adds a line with max. heating and cooling effect
and corresponding hour, and number of hours with
increased ventilation (MAX-vent).

(Other modifications are in preparation).

Hans Lund